

FEA Information Engineering Solutions

Volume 1, Issue 2, March 2012



FEA Information Engineering Solutions:
LS-DYNA Release Notes
ACP 3G Optimization Process
DatapointLabs Mechanical Test Capabilities
Total Human Model For Safety – THUMS



October 2000, FEA Information Inc. published its first monthly newsletter, providing information and solutions related to the evolution of finite element software and current hardware.

Over the years we have expanded to e-mailing the publication to over 7,000 readers, comprised of engineering professionals, professors, consultants, students, and other interested global readers.

1. FEA Information Inc.

- a. FEA Information Engineering Solutions
- b. FEA Information Engineering Journal
- c. FEA Information China Engineering Solutions

FEA Information Engineering Solutions: February, 2000 - The first edition published of FEA Information Engineering Solutions. Initially concentrating on papers already released to the engineering community.

FEA Information China Engineering Solutions February 2012 - The first edition of FEA Information China Engineering Solutions, published in Simplified and Traditional Chinese.

To sign up for the Traditional or Simplified edition write to yanhua@feainformation.com

FEA Information Engineering Journal - February, 2012. The first issue of our Journal publication focusing on published papers and publishing.

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Platinum Participants



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FEA Information
Engineering Journal

FEA Information Engineering Solutions

ANNOUNCEMENTS

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Subject Line: Membership FEA

LSTC

Julia Wolley, LSTC Technical Document Administrator – LS-DYNA release notes are available in pdf format with bookmarks.

FEA Information Inc.

Three publications are now available:

1. FEA Information Engineering Solutions (monthly)
2. FEA Information Engineering Journal (monthly)
3. FEA Information China Engineering Solutions (bi-monthly)

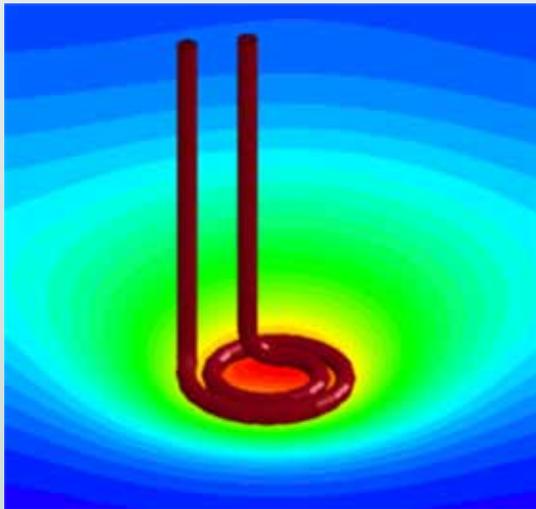
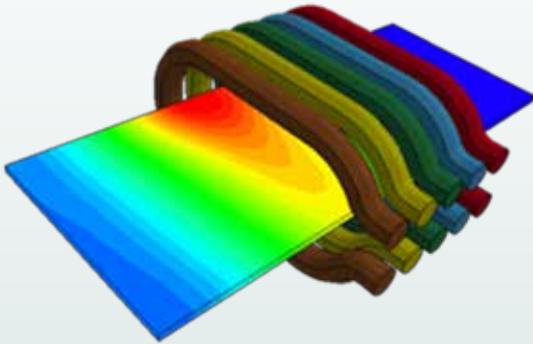
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Cover & Ad Designs by Kanda Choosik

The Electromagnetic solver solves the Maxwell equations in the Eddy current (induction-diffusion) approximation. This is suitable for cases where the propagation of electromagnetic waves in air (or vacuum) can be considered as instantaneous. Therefore, the wave propagation is not solved. The main applications are magnetic metal forming or welding, induced heating, and so forth. The EM module allows the introduction of a source of electrical current into solid conductors and the computation of the associated magnetic field, electric field, as well as induced currents. The EM solver is coupled with the structural mechanics solver (the Lorentz forces are added to the mechanics equations of motion), and with the structural thermal solver (the ohmic heating is added to the thermal solver as an extra source of heat). The EM fields are solved using a Finite Element Method (FEM) for the conductors and a Boundary Element Method (BEM) for the surrounding air/insulators. Thus no air mesh is necessary.



Features

- **Eddy-current solver**
- **Induced heating solver**
- **Resistive heating solver**
- **Uniform Current in Coils**
- **Structure and Thermal coupling**
- **Axisymmetric capabilities**

For further information contact:

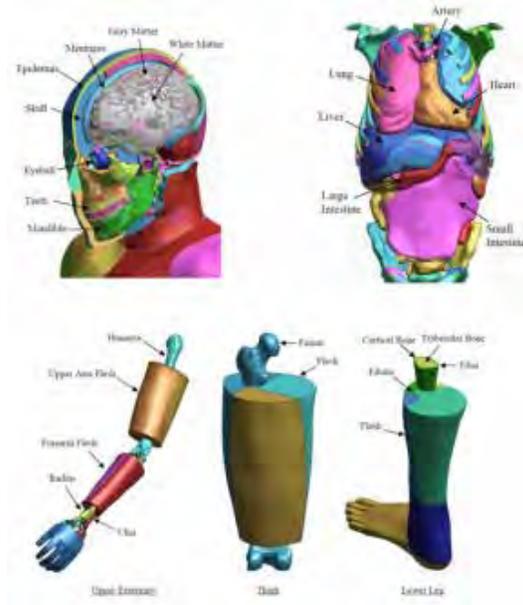
info@lstc.com



About

The Total Human Model for Safety, or THUMS™, is a joint development of Toyota Motor Corporation and Toyota Central R&D Labs. Unlike dummy models, which are simplified representation of humans, THUMS represents actual humans in detail, including the outer shape, but also bones, muscles, ligaments, tendons, and internal organs. Therefore, THUMS can be used in automotive crash simulations to identify safety problems and find their solutions.

THUMS is limited to civilian use and may under no circumstances be used in military applications.



Model Details: The latest Version of the THUMS model is Version 4.

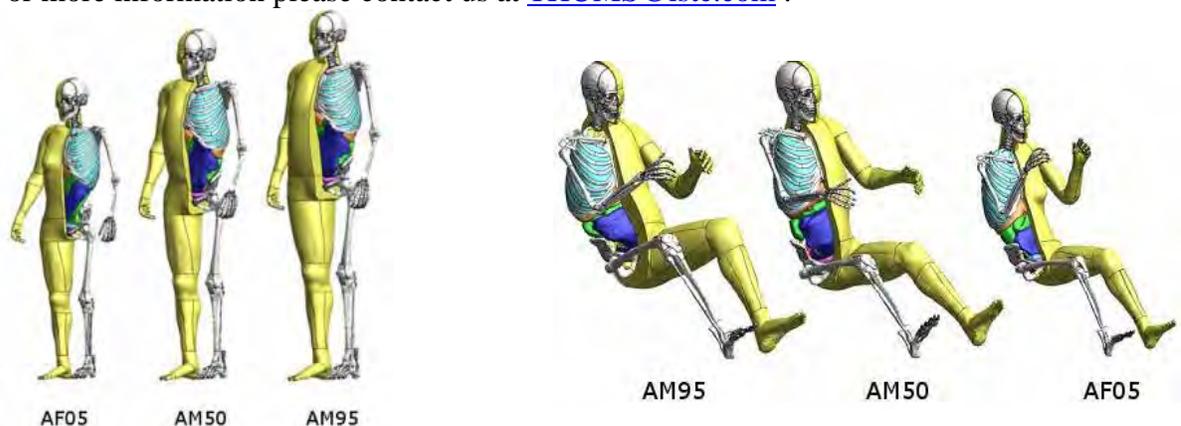
Three different sizes of the model are available:

- Adult female 5th percentile
- Adult male 50th percentile
- Adult male 95th percentile

Each of the different sized models is available as sitting model to represent vehicle occupants and as standing model to represent pedestrians.

The internal organs were modeled based on high resolution CT-scans.

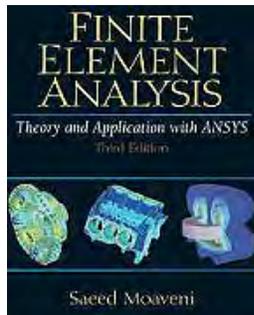
LSTC is the US distributor for THUMS. Commercial and academic licenses are available. For more information please contact us at THUMS@lstc.com.



THUMS™ is a registered trademark of Toyota Central R&D Labs.



Reference Library



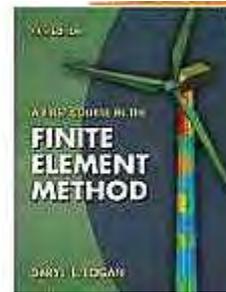
[Finite Element Analysis
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Saeed Moaveni



[Practical Stress
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Bryan J Mac Donald



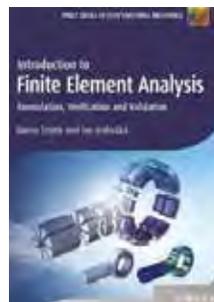
[A First Course in
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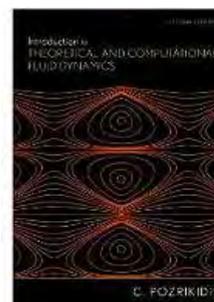
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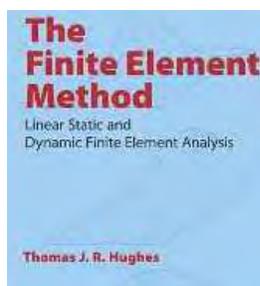
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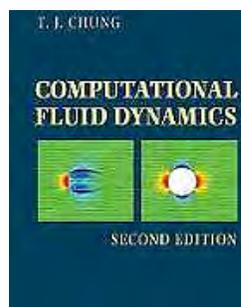
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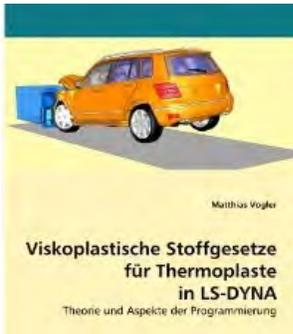
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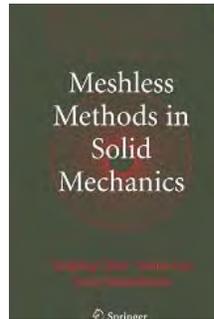
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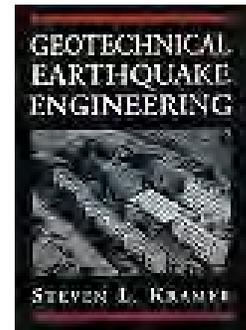
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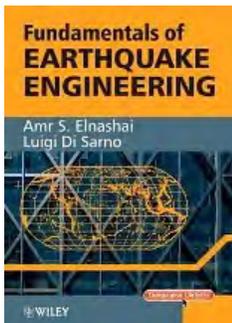
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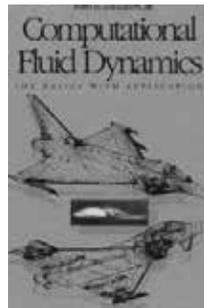
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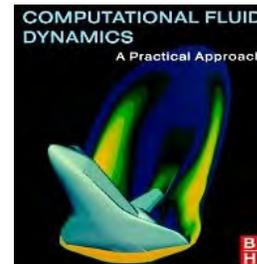
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Guan Heng Yeoh



[Biomechanical Systems Technology: Computational Methods](#)
Cornelius T. Leondes



ACP 3G Optimization Process

The following is an excerpt – the entire white paper is available at ETA:
<http://www.eta.com/images/acp-3g-whitepaper-opt.pdf>

WHITEPAPER - ACP 3G Optimization Process

Authors: Dr. Akbar Farahani, Dir. of Engineering, Paul Dolan, Program Mgr., ETA

Introduction: The design of automotive body structures are driven by many competing criteria such as lower cost, weight reduction, enhanced multi-disciplinary performance, and manufacturability. In addition, the introduction of new manufacturing processes and materials (e.g., AHSS) significantly increases the available design space, or the set of all possible designs for an automotive system.

In order to explore this large design space more effectively while trying to reduce design cycle times, engineers can now take advantage of an automated design optimization process. These tools can greatly decrease the time required to identify a set of feasible, or even near-optimal, designs prior to building and testing the first prototype. Moreover, these tools can also compensate for the limitations of human intuition and provide design engineers with the freedom and power to seek creative solutions that are not obvious to even the most experienced engineer. 3G (Geometry, Grade and Gauge) optimization is the driving force behind ETA's new design process, Accelerated Concept to Product (ACP) [1]. The focus of this white paper is on 3G optimization within the ACP process as applied to a front

longitudinal rail of the FutureSteelVehicle (FSV).

WorldAutoSteel's objective in the FSV program was to develop detailed design concepts and fully optimize a radically different body structure vehicle for production in the 2015-2020 timeframe utilizing the latest grades of advanced and ultra-high strength steels. FSV achieved 35 percent mass reduction at no additional cost over a conventional steel body, while achieving simulated crash test performance with a 5-star safety rating.

Optimization Software Requirements

The process requires an optimization software package that allows designers to automatically and concurrently explore hundreds of design parameters and their relationships in product and process design scenarios, and intelligently seeks optimal values for parameters that affect performance and cost. The software must have non-linear capability enabling interaction with non-linear software (for impact analysis, such as LS-DYNA). Optimization software can be used to improve any engineering system (structural, thermal, fluid, electrical, etc.) including multi-disciplinary scenarios.

For ACP 3G Optimization structural design applications, the HEEDS optimization code can automate the search for designs that simultaneously satisfy the objectives and targets for crashworthiness, manufacturability, mass, cost, stiffness, durability, noise and vibration, robustness and reliability [2].

Parameterization and Design integration (CAD/FEM)

Software with a set of design tools providing detailed parameterization capabilities is required to allow changes in the design's geometry based on optimization recommendations. The new geometry is re-meshed with all the suitably updated joints and then output as a new input deck. It can then be submitted to the appropriate solver (LS-DYNA/NASTRAN/NISA, etc). SFE-Concept offers these capabilities and is used in ACP 3G optimization.

Load path Optimization and 3G (Geometry, Grade and Gauge) Design Optimization

The goal of the ACP 3G Optimization process is to identify the optimal design solution within the available design space. The extent of the design space is defined by three criteria, whose relationship is illustrated in Figure 1.

1. Design Variables -

The combinations design features that the ACP process is free to explore

a. Loadpath

The position of any given structural member [6,2,4]

b. Geometry

The cross-sectional shape of that structure member [3,8,9]

c. Grade

The choice of material that the structural member is made from[5]

d. Gauge

The thickness of material that the structural member is made from[5,7]

2. Design Constraints

Design constraints define the required performance level which the design must meet. For example under multidisciplinary loadings, a design might be required to simultaneously meet a maximum acceleration pulse for the NCAP Front Impact Loading (FMVSS 208), while maintaining a maximum passenger compartment intrusion under IIHS Front Impact Loading. This is a design requirement that places the design responses in direct conflict with each other, revealing one of the ACP's key strengths, its ability to provide a truly balanced solution [3].

3. Design Objective

The goal of the optimization for FSV was to obtain the greatest possible structural efficiency, hence, the lightest design solution.

ACP 3G Optimization Process

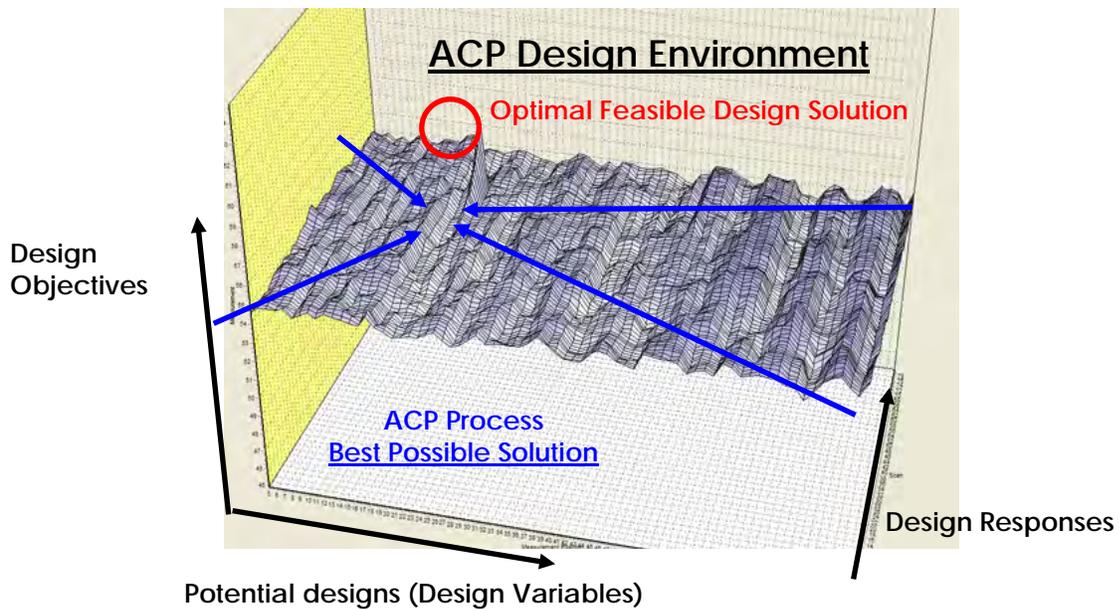


Figure 1: The ACP Design Environment

Figure 1

shows a pictorial representation of the design environment that the ACP process is working within. The first axis defines all possible combinations of the design variables as individual designs. Depending on the total design variable count, this could result in an enormous number of unique designs. The second axis represents the response of each design to the loadcases under consideration. Note that from all possible responses there is a subset of feasible designs that meet the required design constraints. This is the control on the ACP process for it is only the feasible designs that are of interest. The third axis represents how well each design meets the design objective and for FSV, this is the

mass of the BIW. Thus the optimal design is the feasible design that best meets the design goal [9].

When considering the designs generated by the ACP Process it is important to consider the following.

1. Process is a Search Engine

In itself the ACP 3G optimization process is unable to “invent” rather it is searching a design space that has been defined by the user for the best possible solution that meets the design constraints. [9]

2. Enablers

The ACP Process considers in combination all available variables that it is given. As noted previously the ACP process is not able to invent but it does a **high level of balancing**. Therefore, when reviewing the specific design variable selections for a given design it is inappropriate to consider them in isolation. For example, the choice of a particular material grade should not be considered without first understanding the choice of cross-sectional shape and gauge of that component and its relationship to all other components within the structure affected by the same loading condition.

3. Targets

The design constraints define the required performance. The process will seek to find the best possible solution with respect to the design objective, where performance is just good enough.

4. Performance

Depending on the freedom that the process is given, the resulting design

solutions can be very unconventional. However, it should be noted that each design's performance has been measured against the design constraints and so they can confidently be considered a valid design.

FSV Front Longitudinal Rail 3G Sub-System Optimization

Background

The entire vehicle design cycle consisted of 6 major task (T1 to T6) defined below in Figure 2. Figure 2 shows the overall flow of the design process [1].

T1 – Styling and aerodynamics

T2 – Linear static topology optimization

T3 – Non-linear dynamic topology optimization (Low Fidelity 3G (Gauge, Grade, and Geometry) optimization, aka LF3G) full vehicle level

T4 – Sub-system topography optimization (subject of this paper)

T5 – Design confirmation

T6 – Final gauge and grade optimization (full vehicle)

FOR THE FULL WHITE PAPER

<http://www.eta.com/images/acp-3g-whitepaper-opt.pdf>



d3view

www.d3view.com

Visualization of Triaxiality Factor in LS-PrePost

Posted on March 2, 2012 by Suri Bala

Stress Triaxiality is the ratio of Hydrostatic stress and the von-Mises stress and is known to have a great influence on the plastic deformation.

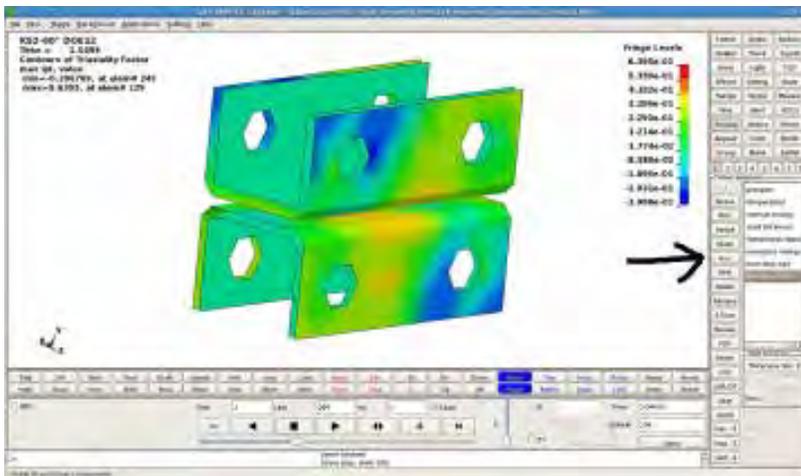
$$\frac{\sigma_h}{\sigma_{eqv}} = TF = \frac{1/3(\sigma_1 + \sigma_2 + \sigma_3)}{\frac{1}{\sqrt{2}}\sqrt{(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2}}$$

where σ_1 , σ_2 and σ_3 are the first, second and third principal stresses and

$$\frac{\sigma_1 + \sigma_2 + \sigma_3}{3} = \text{Hydrostatic stress}$$

$$\frac{1}{\sqrt{2}}\sqrt{(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2} = \text{Equivalent von Mises stress}$$

You can view this factor in LS-PrePost now as shown below at www.d3view.com

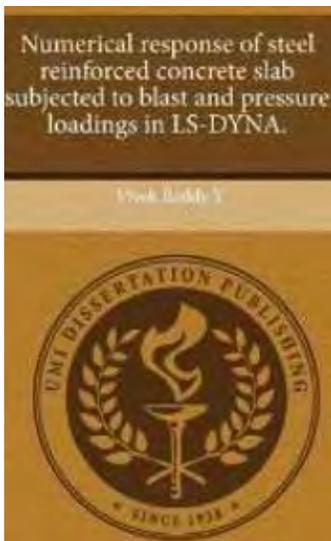




[Numerical response of steel reinforced concrete slab subjected to blast and pressure loadings in LS-DYNA.](#)

[Paperback] –

Author: Vivek Reddy



Publication Date: September 30, 2011

As steel reinforced concrete has got wide range of applications, this project is an attempt to study the dynamic behavior of steel reinforced concrete subjected to blast and pressure loadings using a non-linear finite element code LS-DYNA (version 971).

The aim of this project was to analyze various parameters of a steel reinforced concrete slab by validating three of the concrete material models in LS-DYNA.

The first part of the project consists of validating three concrete material models in LS-DYNA by applying boundary conditions on simple single elements. The next part consists of using these three concrete material models of LS-DYNA (version 971) for the study of blast and pressure load analysis on a steel reinforced concrete slab for two different strengths of concrete with two different mesh sizes.

The main purpose of this analysis was to provide the behavior of these concrete material models subjected to blast loads, which would be a better guide for future applications.



Software Diagnostics Manage Software Projects More Efficiently

www.softwareiagnostics.com

Software Diagnostics

Software Diagnostics is a German company specializing in the areas of software intelligence and software mining. The main focus of the business is on improving the transparency and control of software development and maintenance projects on the basis of their source code reality. With a foundation of over seven years' research work, Software Diagnostics was started in 2009, as a spin-off of the Hasso Plattner Institute – the German university centre of excellence for IT systems engineering.

Software Diagnostics' solutions provide all parties involved in software projects – from company management through to developers – with a valuable basis for decision making through the entire life cycle of a software system. The new software mining process automatically extracts objective information about the software project from a wide variety of sources and then brings it together. Source code parsing, dynamic run time analysis and in particular numerous repositories – such as versioning systems, bug tracking, requirements and test case management systems – are thus, for the first time, meaningfully combined.

Software Diagnostics has developed, amongst other things, an integrated software

intelligence platform which creates automatic management reports (so-called software maps) of the processes within a software project. These provide managers and team leaders with objective and daily updated information on the status of the project. Decision makers thus have at their disposal a tool which can assist them in directing their own developers or external teams, efficiently and in a focused manner.

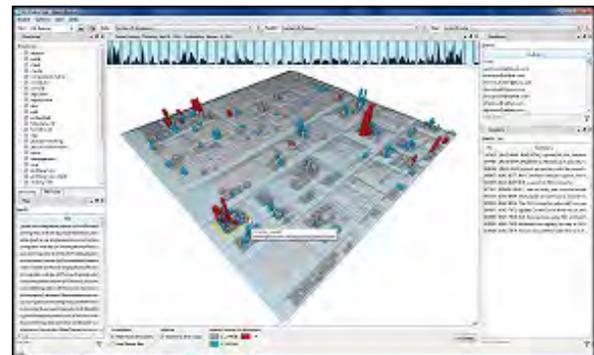


Image 1 shows an example of a software map, revealing the current risks and costs in the source code of a software program with several million lines of code. At a glance, those in charge of the software project can see that particular parts of the source code have been programmed in a monolithic, unstructured and highly complex manner.

Software Diagnostics Manage Software Projects More Efficiently

Each source code file is depicted on the software map as a block and positioned according to the modular structure of the software, the base area of each block corresponding to the number of lines of code in the respective file. A block's color shows its complexity whilst its height reflects how often changes are made. The quality of the sections of code identified as problematic should then be improved as quickly as possible in order to speed up the progress of a project, hampered by code which has become difficult to understand. Furthermore,

the improvement in quality would reduce the existing risk of flawed changes being made within these complex code sections which could lead to considerable costs over the course of the project.

Without a suitable tool, such problematic situations are only discovered after it is too late and the budget and time frame have started to run out of control. In contrast, a software intelligence platform used as an early warning system reveals problem situations as soon as they are created.

Contact Person

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Software Diagnostics GmbH

johannes.bohnet@softwarediagnostics.com

www.softwarediagnostics.com



Oasys LS-DYNA 5th annual Update Meetings India Pune April 17th Bangalore April 19th

Agenda www.oasys-software.com/dyna/en/events/users_india_apr-12/users_india_apr-12.shtml

Oasys Ltd and nHance Engineering Solutions Pvt Ltd are pleased to announce the 5th Oasys LS-DYNA Update meetings in India for the year 2012. First meeting shall be held at **Pune** on Tuesday 17th April 2012 at The Ista Hotel and second meeting shall be held at **Bangalore** on Thursday 19th April 2012 at The Taj Vivanta, Whitefield.

Each of these is a full day free of charge event covering both LS-DYNA and Oasys software and is a perfect opportunity to find out about current and future developments and how the software is being used in the engineering community.

The presentations will mainly cover latest features of LS-DYNA software, Oasys suite and presentations from industry members specifically from OEMs like Mercedes Benz, Tata Motors & General Motors. This year's presentations also include presentation from **Mr. Yun Huang, LSTC on the capabilities of LS-DYNA for NVH and Durability.**

Registration: Please send your registration to this event by email to india.support@arup.com with your name, company/affiliation, telephone number and your choice for event.

Venue: The event in Pune will be held at The Ista Hotel, which is situated in the heart of the city, 10 minute drive from the airport and adjacent to the tranquil Aga Khan Palace.

The Ista Hotel - 88/4, Pune-Nagar Road
(Adj. Aga Khan Palace)
Yerwada Pune - 411 006, India
Tel: 91(20) 41418888

The event in Bangalore will be held at The Taj Vivanta, Whitefield which stands right at the main entrance to the International Tech Park, Bangalore.

The Taj vivanta, ITPB, Whitefield
Bangalore 560 066, India
Tel No.: 91-80-6693-3333

If you plan to stay over before or after the event, we are pleased to confirm that we have negotiated a special rate for attendees of the Oasys LS-DYNA Update meeting. Please contact us for assistance.

Contact Details: If you have any queries regarding this event you can contact:

Mr. Asif Ali
nhance Engineering Solutions(P)Ltd.
Tel: +91 (0) 40 44369797/8
Email: india.support@arup.com



Julia Wolley, LSTC, Technical Administrator, Documentation

LS-DYNA Product Version Release Notes are compiled in text format by Lee Bindeman, and Jim Day of LSTC.

In addition to this original text format, LSTC will be publishing a compilation of these notes in pdf format, with bookmarks.

If you would like to receive the current version in pdf format and be added to the mailing list for future pdf format, please e-mail, jwolley@lstc.com subject line Release Notes.

Release Notes

Product: LS-DYNA®

Version: LS-DYNA version 971 R6.0.0.

Livermore Software Technology Corp. 7374 Las Positas Road, Livermore, CA 94550

LS-DYNA Release Notes

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New Features

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*FREQUENCY_DOMAIN

*INITIAL

*LOAD

*MAT

ALE

SPH

EFG

*IMPLICIT

THERMAL

MPP

FORMING

Discrete Element Method

Isogeometric Elements

Miscellaneous

NEW FEATURES:

Keyword: *AIRBAG_HYBRID, *AIRBAG_WANG_NEFSKE

Added option of not applying pressure to part representing the venting hole.

Keyword: *AIRBAG_PARTICLE

Added BLOCK=10/11 to allow physical hole in the airbag due to eroded shells.

Keyword: *INITIAL_AIRBAG_PARTICLE_POSITION

New command to define initial position of airbag particles.

Keyword: *ALE_REFINE

Keyword to automatically refine the ALE mesh. Each element is replaced by 8 elements if a criteria is reached.

Keyword: **BOUNDARY_RADIATION_SET_VF_CALCULATE_RESTART

Added a new RESTART capability to the radiation view factor calculator as some viewfactor calculations may take hours to weeks (or even months) to calculate.

**Keyword: *BOUNDARY_COUPLED, *DEFINE_SPOTWELD_MULTISCALE,
*INCLUDE_MULTISCALE_SPOTWELD**

Implemented loose coupling with other MPI programs. Currently only useful when linking with MPP LS-DYNA for modeling of multiscale spotwelds.

NEW FEATURES:

Keyword: *CONSTRAINED_LAGRANGE_IN_SOLID

Added parameter POREINI and associated options for computing porosity for CTYPE=11 and 12.

Keyword: *CONSTRAINED_SPR2, *CONSTRAINED_INTERPOLATION_SPOTWELD

Added inverse distance weighting for distribution of motion, forces, and moments (INTP=2).

Keyword: *CONSTRAINED_SPR2

Added option for *CONSTRAINED_SPR2 which enables choice of normals computation: ALPHA3.gt.0: incremental update (default), ALPHA3.lt.0: total update (new).

Keyword: *CONTACT_TIED_..., *CONTROL_ADAPTIVE

Allowed for tied contacts in MPP with solid remeshing: the interfaces are completely re-initialized after each adaptive step, which is fine for constraint type contacts, but penalty types might experience accumulated drift/creeping and force discontinuities.

Keyword: *CONTACT_2D_AUTOMATIC_SURFACE_TO_SURFACE

Implemented a user defined curve for the penalty stiffness like in *CONSTRAINED_LAGRANGE_IN_SOLID. If SFACT<0, abs(SFACT) is ID of the curve providing pressure-vs-penetration.

Keyword: *CONTACT_..._ORTHO_FRICTION

Added another method to specify orthotropic friction in contact but which is available in SMP and MPP.
See also *DEFINE_FRICTION_ORIENTATION (SMP only).

Keyword: *CONTACT_SPOTWELD_WITH_TORSION_PENALTY

Added penalty formulation to spotweld_with_torsion contact in both explicit and implicit.

NEW FEATURES:

Keyword: *CONTROL_IMPLICIT_EIGENVALUE

Added postprocessing of eigenforms of isogeometric elements to d3eigv for MPP.

Keyword: *CONTROL_MPP_CONTACT_GROUPABLE

Added control command to invoke groupable contact.

Keyword: *CONTROL_RIGID

Added plot element generation parameter (PLOTTEL) for nodal rigid bodies.

Keyword: *CONTROL_IMPLICIT_GENERAL

Added geometric stiffness for type 6 beam.

Keyword: *CONTROL_FORMING_PRE_BENDING

Added *CONTROL_FORMING_PRE_BENDING to allow blank to be prebent prior to gravity loading.

Keyword: *CONTROL_FORMING_ONESTEP_option

Added new feature for one-step forming simulation that determines an unformed blank size and thickness, and also provides stress/strain/thickness of formed part for initialization in crash analysis.

Option AUTO_CONSTRAINT allows nodal restraints to be applied automatically in implicit calculation to prevent rigid body motion.

Option DRAWBEAD is used for application of extra draw bead forces.

Option FRICTION applies friction along the periphery of the part, based on a user input “binder pressure”.

Keyword: *CONTROL_SHELL

Allowed the ISTUPD thickness update option to be invoked by part ID.

Keyword: *DATABASE_BINARY_CPMFOR

Added binary output database for *AIRBAG_PARTICLE coupling surfaces.

There are four components in the database, coupling pressure, fx, fy and fz.

NEW FEATURES:

Keyword: *DATABASE_FREQUENCY_BINARY_...

Added frequency range for d3psd in *DATABASE_FREQUENCY_BINARY_D3PSD.
Added frequency range for d3ssd in *DATABASE_FREQUENCY_BINARY_D3SSD.
Added command *DATABASE_FREQUENCY_BINARY_D3RMS.
Added command *DATABASE_FREQUENCY_BINARY_D3FTG.
Added command *DATABASE_FREQUENCY_BINARY_D3SSD.
Added command *DATABASE_FREQUENCY_BINARY_D3PSD.
Added command *DATABASE_FREQUENCY_BINARY_D3ACS.
Added command *DATABASE_FREQUENCY_BINARY_D3SPCM.

Keyword: *DATABASE_BINARY_FSIFOR

Added three additional components to the binary fsifor database, namely, the x, y, and z components of relative tangential velocity.

Keyword: *DATABASE_TRACER

Added NID parameter for assigning location of tracer by a massless node ID.

Keyword: *DATABASE_DISBOUT

Implemented ASCII output file for discrete beams which includes relative displacements, rotations, force resultants, and orientation of the local coordinate system.

Keyword: *DATABASE_CPM_SENSOR

Added cylindrical shape CPM sensor to get better pressure signal.

Allowed user to select a disk region near the segment in CPM sensor to collect more particle data and get much smoother signal from CPM.

Keyword: *DEFINE_COORDINATE_SYSTEM

Added local coordinate system option CIDL to *DEFINE_COORDINATE_SYSTEM.

Keyword: *DEFINE_CURVE_FUNCTION

Implemented the Arithmetic IF conditional for *DEFINE_CURVE_FUNCTION.

NEW FEATURES:

Keyword: *DEFINE_BOX_SPH

Added a new option for DEFINE_BOX_SPH where by the box follows a node.

Keyword: *DEFINE_CURVE_FUNCTION

Added "sensor" to list of functions for *DEFINE_CURVE_FUNCTION so that *SENSOR_CONTROL may affect a curve.

Keyword: *DEFINE_CPM_BAG_INTERACTION

Added a new feature that allows the cpm particles vented from the master bag to be the input mass flow for the slave bag.

Keyword: *ELEMENT_BEAM_PULLEY

Added *ELEMENT_BEAM_PULLEY for the definition of a pulley for truss beam elements (see *SECTION_BEAM, ELFORM=3). Currently, the beam pulley is implemented for *MAT_001 and *MAT_156. Pulleys allow continuous sliding of a string of truss beam element through a sharp change of angle.

Keyword: *ELEMENT_MASS_MATRIX

Added treatment of nodal mass matrices to implicit via *ELEMENT_MASS_MATRIX.

Keyword: *ELEMENT_SEATBELT_SLIPRING

Added normal-force-dependent slipping friction.

Keyword: *ELEMENT_TSHELL_COMPOSITE

Added *ELEMENT_TSHELL_COMPOSITE which allows an arbitrary number of through-thickness integration points to be defined in tshell elements that share the same part ID.

Keyword: *HOURGLASS

Added hourglass formulation 10. Solid element formulation 1 with hourglass formulation 10 is a Cosserat point element, see M. Jabareen and M.B. Rubin, 'A Generalized Cosserat Point Element (CPE) for Isotropic Nonlinear Elastic Materials including Irregular 3-D Brick and Thin Structures', J. Mech. and Mat. Struct., Vol 3 (2008) pp. 1465-1498.

NEW FEATURES:

Keyword: *INITIAL_STRESS_SPH

Implemented initial stress command for SPH.

Keyword: *INTERFACE_SPRINGBACK, *INITIAL_STRAIN_SHELL

Made strain at all integration points available for MPP adaptive jobs.

Added output of strain at all integration points to dynain and dynain.bin.

Keyword: *LOAD_THERMAL_D3PLOT

Replaced *LOAD_THERMAL_TOPAZ with *LOAD_THERMAL_D3PLOT which allows temperatures from a thermal-only analysis to be used in a structural- only analysis.

Keyword: *MAT_015

Added NUMINT parameter for failure of *MAT_JOHNSON_COOK shells.

Keyword: *MAT_036, *MAT_133

Added heat treatment flag in *MAT_3-PARAMETER_BARLAT and *MAT_BARLAT_YLD2000.

Imposes changes in yield and hardening properties due to local or global heating to simulate enhanced formability in aluminium sheets.

Keyword: *MAT_054

Added new material parameter SOFTG to *MAT_ENHANCED_COMPOSITE_DAMAGE intended to soften GBC and GCA in crashfront elements.

Keyword: *MAT_100

Added option to fail all spotweld elements in an assembly simultaneously when one of the elements reaches the failure strain.

Keyword: *MAT_133

Added Gosh and Hockett-Sherby hardening to *MAT_BARLAT_YLD2000.

Keyword: *MAT_181

Added *MAT_SIMPLIFIED_RUBBER/FOAM for truss elements.

Keyword: *MAT_208

Implemented *MAT_BOLT_BEAM for discrete beams.

NEW FEATURES:

Keyword: *MAT_219

Added *MAT_CODAM2 for shell, thick shell and brick elements.

Keyword: *MAT_220

Implemented use of shells for *MAT_RIGID_DISCRETE.

Keyword: *MAT_224

Added temperature dependent Young's modulus for *MAT_TABULATED_JOHNSON_COOK. Negative value of E is now interpreted as a curve.

Keyword: *MAT_246

Implemented *MAT_PML_NULL - PML material for MAT_NULL with EOS_1 or 4.

Keyword: *MAT_ADD_AIRBAG_POROSITY_LEAKAGE

Added command to specify porosity leakage for non-fabric material in control volume modeled with *AIRBAG_HYBRID and *AIRBAG_WANG_NEFSKE.

Keyword: *MAT_NONLOCAL

Updated nonlocal smoothing (*MAT_NONLOCAL) to support thick shell elements in addition to shell and solid elements. Also enabled fully integrated elements to be properly smoothed. The MPP version now fully supports *MAT_NONLOCAL.

Keyword: *MAT_ADD_EROSION

Added new thinning strain failure criterion (EPSTHIN).

NEW FEATURES:

Keyword: n/a

Added -j option to l2a so as to retain binout prefix in ASCII output files.

Keyword: n/a

Added check in MPP of installed memory on system and requested memory. If requested memory exceeds the real memory, the job will terminate unless command line option swapping=yes is on. This avoids some system crashes due to exhausted resources.

Keyword: *PART_..._AVERAGED

Added AVERAGED option for truss elements so all the elements have the same force.

Keyword: *RIGIDWALL_PLANAR

Added DISPLAY option to *RIGIDWALL_PLANAR as means to display the wall.

Keyword: *SECTION_TSHELL, *CONTROL_ACCURACY

Added support for objective stress update for all tshell formulations.

Keyword: *SECTION_SOLID

Added 1-point pentahedron element (ELFORM=115) with F-B hourglass control for implicit and explicit.

Keyword: *SENSOR_DEFINE_..._SET

Added option of "set" to *sensor_define_node and *sensor_define_element.

Keyword: *SET_SEGMENT_ADD, *SET_SEGMENT_INTERSECT.

Added keywords *SET_SEGMENT_ADD and *SET_SEGMENT_INTERSECT.

***AIRBAG - LS-DYNA version 971 R6.0.0.**

Keyword: *AIRBAG_HYBRID, *AIRBAG_WANG_NEFSKE

Allowed venting and porosity parameters to be defined using *DEFINE_CURVE_FUNCTION.

Keyword: *AIRBAG_PARTICLE

Removed encrypted *AIRBAG_PARTICLE data from d3hsp.

Keyword: *AIRBAG_PARTICLE

Assigned reference chamber ID for *AIRBAG_PARTICLE.
Fixed bug if chamber option and initial air option are both defined.

Keyword: *AIRBAG_PARTICLE

Improved computational efficiency of CPM chambers.

Keyword: *AIRBAG_PARTICLE

Enabled PPOP in *AIRBAG_PARTICLE for opening internal vent holes due to internal/external pressure differential.

Keyword: *AIRBAG_WANG_NEFSKE

Output airbag porosity leakage and venting hole leakage separately when CV=0.

Keyword: *DATABASE_CPM_SENSOR

Added option for CPM sensor to monitor rectangular box.

Keyword: *DEFINE_CPM_BAG_INTERACTION

Fixed bug affecting multiple definitions of CPM airbag interaction.

Keyword: *SENSOR_CONTROL

Fixed broken *SENSOR_CONTROL type 'AIRBAG' when airbag is defined with *AIRBAG_PARTICLE.

***BOUNDARY - LS-DYNA version 971 R6.0.0.**

Keyword: *BOUNDARY_CYCLIC

Added SMP and MPP support for multiple sets of cyclic boundary conditions.

Added ID option to *BOUNDARY_CYCLIC for id numbers and titles.

Keyword: *BOUNDARY_PRESCRIBED_ACCELEROMETER

Improved load curve parity check for *BOUNDARY_PRESCRIBED_ACCELEROMETER.

Keyword: *BOUNDARY_PRESCRIBED_FINAL_GEOMETRY

Added *BOUNDARY_PRESCRIBED_FINAL_GEOMETRY to implicit.

Keyword: *BOUNDARY_PRESCRIBED_ORIENTATION_RIGID

Fixed MPP explicit handling of subject command.

Keyword: *BOUNDARY_PRESCRIBED_ACCELEROMETER

Fixed acceleration output to rbdout for *BOUNDARY_PRESCRIBED_ACCELEROMETER.

Keyword: *BOUNDARY_PRESCRIBED_MOTION_RIGID

Fixed problem of nodal rigid bodies not moving when

*BOUNDARY_PRESCRIBED_MOTION_RIGID is used with DOF=9/10/11 or VAD=4.

Keyword: *BOUNDARY_PRESCRIBED_MOTION_SET

Corrected bug affecting *SENSOR when used to control

*BOUNDARY_PRESCRIBED_MOTION_SET.

Keyword: *BOUNDARY_PRESCRIBED_ORIENTATION_RIGID

Fixed implicit MPP implementation of *BOUNDARY_PRESCRIBED_ORIENTATION_RIGID.

Keyword: *BOUNDARY_SPC

Fixed bug whereby spc constraint got lost after trimming.

Keyword: *BOUNDARY_USA_SURFACE

Fixed bug involving USA and dynamic relaxation

***CONSTRAINED - LS-DYNA version 971 R6.0.0.**

Keyword: *CONSTRAINED_COORDINATE

Fixed bug.

Keyword: *CONSTRAINED_COORDINATE, *DATABASE_SPCFORC

Fixed the capturing of resultant forces for *CONSTRAINED_COORDINATE in implicit.

Keyword: *CONSTRAINED_INTERPOLATION

Improved error handling for when SGESVD fails for either
*CONSTRAINED_INTERPOLATION_LOCAL or _GLOBAL.

Keyword: *CONSTRAINED_INTERPOLATION

Fixed bug affecting *CONSTRAINED_INTERPOLATION in MPP implicit.

Keyword: *CONSTRAINED_JOINT_STIFFNESS_GENERALIZED

Extended the rotation angle of *CONSTRAINED_JOINT_STIFFNESS_GENERALIZED to allow initialization to +/- 180 degrees. Previously, phi and theta could initialize to only +/- 90. This change applies to the incremental update option (JNTF=0 on *CONTROL_RIGID).

Keyword: *CONSTRAINED_JOINT_STIFFNESS_...

Fixed problem of *CONSTRAINED_JOINT_STIFFNESS remaining in effect after joint fails.

Keyword: *CONSTRAINED_LAGRANGE_IN_SOLID

Added in support for thick shell parts as slave.

Keyword: *CONSTRAINED_LINEAR_...

Fixed bug in *CONSTRAINED_LINEAR... if rotational DOF is specified.

***CONSTRAINED - LS-DYNA version 971 R6.0.0.**

Keyword: *CONSTRAINED_RIGID_BODY_STOPPER

Fixed problem affecting *CONSTRAINED_RIGID_BODY_STOPPER with VID=4 or 8.

Keyword: *CONSTRAINED_SHELL_TO_SOLID

Fixed bug encountered when 9 solid nodes are included in NSID.

Keyword: *CONSTRAINED_SPR2, *CONSTRAINED_INTERPOLATION_SPOTWELD

Fixed for rare appearance of accuracy issues in single precision

Keyword: *CONTACT

Segment based contact (SOFT=2 on optional card A) has been observed to be slower than R4.2 and R4.2.1. The slowdown, first noticed in R5.0, occurs when there are significant numbers of shells in contact that have thicknesses that are large relative to their edge lengths. In older, faster versions, the bucket sort was sometimes not sufficiently robust to identify thick segment pairs in time to treat contact with correct thickness offsets. In R5.0 and later, this is corrected, with the side effect that the bucket sort creates longer lists and the solution time is increased. However, if SHLEDG=1 on *CONTROL_CONTACT, this slowdown does not occur and new versions should run at similar speed to R4.2.

Keyword: *CONTACT_...

Added option to turn off near contact stiffness option in implicit after n cycles. Set IGAP>2.

Keyword: *CONTACT_...

Fixed the neighbor segment checking (SFNBR>0) of segment based (SOFT=2) contact so it works when edge-edge checking is not active (DEPTH .ne. 5,25,35).

Keyword: *CONTACT

Excluded shell edge contact in MPP if edges are from the same segment.

Keyword: *CONTACT

Fixed a segment based (SOFT=2) contact bug that could allow very thick parts to penetrate before contact is detected.

***CONTACT - LS-DYNA version 971 R6.0.0.**

Keyword: *CONTACT_...

Replaced the check for initial penetration in segment based (SOFT=2) contact with a more accurate check that will not report nonsensical values.

Added a new optional card E for *CONTACT in order to add a new parameter for segment based (SOFT=2) contact.

By default, the segment pairs that share rigid bodies, or share nodal constraints, are removed from consideration of contact.

This can cause penetration because 1 or 2 nodes of a segment may belong to a constraint or rigid body, but the other nodes may be in motion, causing the segment to be penetrated.

When the new parameter (ISHARE) in field one of optional card E is set to 1, the sharing of constraints is no longer used to eliminate segment pairs and contact checking is done.

Keyword: *CONTACT_AUTOMATIC_BEAMS_TO_SURFACE

Fixed bug whereby *CONTACT_AUTOMATIC_BEAMS_TO_SURFACE did not work correctly if it was not the first contact surface defined.

Keyword: *CONTACT_AUTOMATIC_GENERAL

Fixed incorrect sliding energy for beam contact.

Keyword: *CONTACT_AUTOMATIC_GENERAL

Computed frictional energy for sleout when using *CONTACT_AUTOMATIC_GENERAL.

Keyword: *CONTACT_AUTOMATIC_..._TIEBREAK

Fixed issues with MPP implementation of AUTOMATIC_TIEBREAK option 5.

Keyword: *CONTACT_2D_AUTOMATIC_...

Fixed 2D automatic contact for explicit solutions. When the velocity of penetration was very slow, it was failing to detect and prevent it.

Keyword: *CONTACT_2D_AUTOMATIC_TIED_...

For 2D adaptive problems with tied contact, now print a tied contact report after each adaptive remesh to the message file.

Keyword: *CONTACT_ERODING_...

Enabled segment based (SOFT=2) eroding contact to work with a segment set for the slave or master side. In this way, eroding can be disregarded on one side or the other, thereby saving resources.

Keyword: *CONTACT_FORCE_TRANSDUCER_PENALTY

Fixed a bug in 2 surface force transducers when used with segment based (SOFT=2) contact.

Keyword: *CONTACT_INTERFERENCE_...

Increased depth of penetration allowed for *CONTACT_INTERFERENCE in MPP.

Keyword: *CONTACT_..._MORTAR

Fixed bugs in mortar contact.

Keyword: *CONTACT_..._MORTAR

Fixed bug in mortar contact.

Keyword: *CONTACT_..._MORTAR

Added edge treatment in mortar contact.

Keyword: *CONTACT_NODES_TO_SURFACE, *USER_INTERFACE_FRICTION

Fixed bug in user friction routine if *CONTACT_NODES_TO_SURFACE is used.

Keyword: *CONTACT_..._TIEBREAK

Issued warning about AUTOMATIC_TIEBREAK types < 0 (which are not supported in MPP) and switch to the corresponding positive type.

Keyword: *CONTACT_TIED_...

Enabled spot weld thinning for tied contact options OFFSET, BEAM_OFFSET, and CONSTRAINED_OFFSET in MPP. Previously, with spot weld thinning turned on via SPOTHIN in *CONTROL_CONTACT, contact thinning was based on proximity to part tied only with *CONTACT_SPOTWELD.

***CONTACT - LS-DYNA version 971 R6.0.0.**

Keyword: *CONTACT_TIBREAK_SURFACE_TO_SURFACE

Added warning for unsupported option TBLCID in
*CONTACT_TIBREAK_SURFACE_TO_SURFACE for MPP.

Keyword: *CONTACT_TIED_..._CONSTRAINED_OFFSET

Fixed serious instability in MPP implementation of subject keyword
and also a fix for tied contacts and adaptivity.

Keyword: *CONTACT_TIED_SHELL_EDGE_TO_SURFACE_OFFSET

Fixed MPP rotational stiffness of
*CONTACT_TIED_SHELL_EDGE_TO_SURFACE_OFFSET i in implicit.

Keyword: *CONTROL_CONTACT

Added new parameter to field 8 of card 6 of *CONTROL_CONTACT
to limit the number of constrained tied nodes that can be deleted before the model
terminates with an error.

Keyword: *CONTROL_DYNAMIC_RELAXATION

Enabled IDRFLG=2 on *CONTROL_DYNAMIC_RELAXATION to be
used with segment based (SOFT=2) interference contact.

Keyword: *DATABASE_BINARY_INTFOR

Fixed a problem of noisy output to intfor in MPP.

Keyword: *DEFINE_FRICTION

Fixed *DEFINE_FRICTION: DC and VC was swapped in the keyword reader in
case PSET was used in PTYPEI/PTYPEJ.

Keyword: *DEFINE_CURVE_ENTITY

Fixed bugs affecting *DEFINE_CURVE_ENTITY when scale
factors/offsets are used or the first point of the curve is not (0,0).

Keyword: *CONTROL_ADAPTIVE, *CONTACT_DRAWBEAD

Fixed bug in adaptivity if the input contains drawbeads.

Keyword: *CONTROL_ADAPTIVE

Fixed the problem of erosion of solid elements being turned off when *CONTROL_ADAPTIVE is used (excludes EFG).

Keyword: *CONTROL_DYNAMIC_RELAXATION

Fixed related to distortional KE when IDRFLG=3.

Keyword: *CONTROL_FORMING_PARAMETER_READ

Fixed problems in first adaptive step when keyword used multiple times.

Keyword: *CONTROL_SOLID

Extended ESORT parameter.

ESORT=1, sort tets to type 10, penta to type 15

ESORT=2, sort tets to type 10, penta to type 115

ESORT=3, sort tets to type 10, penta to type 15, print elements that have switched

ESORT=4, sort tets to type 10, penta to type 115, print elements that have switched

Keyword: *CONTROL_TIMESTEP

Corrected acceleration output for selective mass scaling.

Keyword: *CONTROL_TIMESTEP

Fixed bug whereby selective mass scaling did not consider deletion of rigid bodies.

Keyword: *RIGIDWALL_GEOMETRIC_..., *CONTROL_TIMESTEP

Supported geometric rigid walls in selective mass scaling.

***DATABASE - LS-DYNA version 971 R6.0.0.**

Keyword: *CONTROL_OUTPUT

Fixed broken display of tetrahedrons when TET10=1 in *CONTROL_OUTPUT.

Keyword: *CONTROL_OUTPUT, *DAMPING_GLOBAL

Made clear in d3hsp that whenever *DAMPING_GLOBAL is used, the nodal accelerations output to nodout are averaged over the output interval.

Keyword: *DATABASE

Fixed strain output for shell formulation 18.

Keyword: *DATABASE_ABSTAT

Output airbag interaction energy from master to slave bag to "reaction" field of abstat_cpm data written to binout.

Keyword: *DATABASE_AVSLFT/MPGS/MOVIE

Added error message if *DATABASE_EXTENT_AVS/MPGS/MOVIE is missing.

Keyword: *DATABASE_BINARY_...

Fixed SMP issue of missing d3plot states in small restart.

Fixed MPP issue of corrupt d3thdt data after second restart.

Keyword: *DATABASE_BINARY_D3PART

Fixed corrupt d3part database.

Keyword: *DATABASE_BINARY_D3PLOT

Fixed problem of MPP not properly continuing d3plot on restart.

Keyword: *DATABASE_BINARY_D3PLOT

Fixed bug in output of strain for 2D models.

*mat

Keyword: *DATABASE_BINARY_BLSTFOR

Allowed output interval to be specified with a load curve.

Keyword: *DATABASE_BINARY_INTFOR

Connected implicit mechanics with the intfor file.

Keyword: *DATABASE_BINARY_INTFOR

Automatically reset contact print flags to 0 for *CONTACT_ERODING_... if user sets either flag to 1. The intfor database is not supported for eroding contacts.

Keyword: *DATABASE_BINARY_INTFOR

Fixed bug in intfor for SMP version if it is a thermal problem.

Keyword: *DATABASE_BINARY_INTFOR

Fixed bug in intfor for SMP if thermal solver is invoked.

Keyword: *DATABASE_BINARY_INTFOR

Fixed broken intfor output in MPP.

Keyword: *DATABASE_ELOUT

Fixed miscellaneous bugs in eloutdet output.

*new

Keyword: *DATABASE_ELOUT

Added option for extra history variable output for all integration points to elout.

Keyword: *DATABASE_EXTENT_BINARY, *MAT_002

Corrected the CMPFLG output option for bricks comprised of *MAT_002. The transformation matrix used to output in the local system was not being updated to account for element rotation.

***DATABASE - LS-DYNA version 971 R6.0.0.**

Keyword: *DATABASE_GLSTAT

Also write part number when writing element ID and element time step to glstat and d3hsp.

Keyword: *DATABASE_MATSUM

Output internal energies for each ALE2D group to matsum (like in 3D).

Keyword: *DATABASE_PROFILE

Upgraded *DATABASE_PROFILE for plotting distribution of an element or node component along x,y, or z-direction.

Keyword: *DATABASE_RCFORC

Fixed bug in output of rforc data for implicit.

Keyword: *DATABASE_RCFOR

Fixed bug whereby incorrect forces were gathered by the RCFORC function of *DEFINE_CURVE_FUNCTION.

Keyword: *DATABASE_SLEOUT

Fixed frictional energy output to sleout for implicit.

Keyword: *DATABASE_SPCFORC

Fixed implicit's output of spcforc for linear problems.

Keyword: *DATABASE_SWFORC

Fixed swforc output errors for hex spotweld assembly in MPP.

Keyword: *DATABASE_SWFORC, *MAT_100

Fixed brick and brick assembly spot weld output to the swforc file when welds have failed after damage initiation by either plastic strain or the failure function. This was fixed for all failure options except opt 8 (DAMILER) or option 12 (user defined failure).

Keyword: *ELEMENT_MASS_PART, *DATABASE_MATSUM

Fixed incorrect rigid body velocity and kinetic energy in matsum file when *ELEMENT_MASS_PART is used.

***DATABASE - LS-DYNA version 971 R6.0.0.**

Keyword: *PART_COMPOSITE

Fixed stress output to d3plot for *PART_COMPOSITE. Stresses for some int pts were zero.

Keyword: *MAT_169

Plastic strain rate (edotp) is now stored as extra history var#6 in *MAT_ARUP_ADHESIVE.

***ELEMENT - LS-DYNA version 971 R6.0.0.**

Keyword: *CONTROL_ACCURACY, *SECTION_SOLID

Corrected pentehedral (form 15) brick element when used with invariant node numbering. The symptom was a lack of parallel consistency, but the real problem was an incorrect calculation of the transformation matrix so the behavior of ortho/anisotropic materials was incorrect.

Keyword: *DAMPING_PART_STIFFNESS

Fixed stiffness damping to work correctly for solids.

Keyword: *EOS_USER_DEFINED

Fixed bug associated with *EOS_USER_DEFINED in combination with ELFORM4 tetrahedrons.

Keyword: *ELEMENT_SHELL_NURBS_PATCH, *ELEMENT_GENERALIZED_SHELL

Renamed *ELEMENT_NURBS_PATCH_2D to *ELEMENT_SHELL_NURBS_PATCH
Activate *MAT_24 for isogeometric and generalized shells.

Keyword: *INITIAL_STRESS_SOLID

Fixed reading of initial stresses for pentahedrons.

Keyword: *SECTION_TSHELL

Fixed problem of tshells not always eroding after reaching failure criterion.

Keyword: *SECTION_SHELL, *SECTION_SOLID

Fixed problem whereby 1-point 3D solid elements and 2D solid elements could generate strain during rigid body motion when using single precision.

Keyword: *SECTION_SHELL

Corrected bug in shell formulations 23 and 24 affecting result in pure bending.

Keyword: *SECTION_SHELL

Fixed stress output for triangular shell formulation 17.

Fixed output issues for shell element types 18, 23 and 24.

Keyword: *SECTION_SHELL

Fixed bug in output of shell element type 18 (linear DK).

Keyword: *SECTION_SHELL

Added output of strain for 6-node triangular shell and 8-node quad shell (shell formulations 23 and 24).

Also Fixed implicit formulation of these shells.

Keyword: *SECTION_SHELL

Improved load distribution in quadratic shell formulations 23 and 24.

Keyword: *SECTION_SHELL

Fixed for thickness update of generalized and isogeometric shells.

Keyword: *SECTION_SHELL

Fixed bug in rotation of fibers in shell formulations 23 and 24, and allow mid side nodes to take part in rigid body.

Keyword: *SECTION_SHELL, *MAT_138, *MAT_240

Fixed bug affecting 2D cohesive elements (*SECTION_SHELL, ELFORM=46/47) comprised of *MAT_COHESIVE_MIXED_MODE or *MAT_COHESIVE_MIXED_MODE_ELASTOPLASTIC_RATE.

Keyword: *SECTION_TSHELL, *MAT_USER_DEFINED_MATERIAL_MODELS

Fixed thick shell forms 3 and 5 when used with user defined materials that have orthotropic properties defined (IORTHO=1). Without the fix, the strain increment, stress and deformation gradient transformations are incorrect.

***ELEMENT - LS-DYNA version 971 R6.0.0.**

Keyword: *SECTION_TSHELL, *CONTROL_PARALLEL

Fixed SMP parallel consistency when PARA=1 in *CONTROL_PARALLEL for thick shell forms 3 and 5, brick form 18, tet form 13.

Keyword: *SECTION_SOLID

Slightly modified implicit elform3 to make it compatible with explicit elform3.

Keyword: *SECTION_SOLID

Fixed the deformation gradient calculation for linear solid element type 18. A test case with material 123 was calculating material failure in the first cycle.

Keyword: *SECTION_SOLID, *DATABASE_GLSTAT

Fixed spurious kinetic energy growth in glstat data of elform4 tets.

Keyword: *SECTION_SOLID

Added clean error termination when wrong solid element formulation is specified for 10-noded tetrahedrons.

Keyword: *SECTION_SOLID

Improved accuracy of solid element type 13 (tetrahedron).

***FREQUENCY_DOMAIN - LS-DYNA version 971 R6.0.0.**

Keyword: *DATABASE_FREQUENCY_...

Fixed bug in defining output frequency curve for frequency domain databases.

Keyword: *FREQUENCY_DOMAIN_ACOUSTIC_BEM

Fixed BEM acoustics when using set_segment for acoustic field nodes.

Keyword: *FREQUENCY_DOMAIN_ACOUSTIC_BEM

Added a fringe plot option to all the BEM acoustic solvers.

Updated BEM acoustics to remove the limitation on number of acoustic field nodes.

Keyword: *FREQUENCY_DOMAIN_ACOUSTIC_BEM

Fixed a bug in restarting bem acoustics with SSD response.

Keyword: *FREQUENCY_DOMAIN_ACOUSTIC_FEM

Updated frequency domain fem acoustics to introduce free pressure boundary condition.

Keyword: *FREQUENCY_DOMAIN_ACOUSTIC_FEM

Updated frequency domain fem acoustics, to allow using the results of i transient analysis.

Keyword: *FREQUENCY_DOMAIN_ACOUSTIC_FEM

Fixed frequency domain FEM acoustics for tetrahedrons.

Keyword: *FREQUENCY_DOMAIN_ACOUSTIC_FEM

Added Press_Pa_real and Press_Pa_imag output to frequency domain fem acoustics.

Keyword: *FREQUENCY_DOMAIN_FRF

Fixed a bug in FRF computation with pressure load.

Keyword: *FREQUENCY_DOMAIN_FRF

Extended FRF to base velocity and base displacement excitation.

***FREQUENCY_DOMAIN - LS-DYNA version 971 R6.0.0.**

Keyword: *FREQUENCY_DOMAIN_RANDOM_VIBRATION

Added xyplot output of psd_curve_print, converted from time history load, for random vibration LDTYP=2.

Keyword: *FREQUENCY_DOMAIN_RANDOM_VIBRATION

Fixed bug in reading mode information in random vibration.

Keyword: *FREQUENCY_DOMAIN_RANDOM_VIBRATION

Fixed bug in reading modal information and writing d3rms in random vibration analysis.

Keyword: *FREQUENCY_DOMAIN_RANDOM_VIBRATION_FATIGUE

Added the option to define SN fatigue curves by two equations, for random fatigue.

Implemented Dirlik method to random fatigue analysis (mode acceleration only).

Keyword: *FREQUENCY_DOMAIN_RESPONSE_SPECTRUM

Added Double Sum method to response spectrum analysis (MCOMB=3).

Keyword: *FREQUENCY_DOMAIN_SSD

Fixed bug in SSD with multiple excitations.

Fixed bug in SSD when using local damping option.

Keyword: *FREQUENCY_DOMAIN_SSD

Updated on SSD to allow multi-axial excitation.

Keyword: *FREQUENCY_DOMAIN_SSD

Added output of beam integration point values in Steady State Dynamics.

Keyword: *FREQUENCY_DOMAIN_SSD

Fixed a bug in writing nodout_ssd and elout_ssd files.

Keyword: *INITIAL_STRESS_SOLID

Added transformation of solid stresses input with *INITIAL_STRESS_SOLID when *INCLUDE_TRANSFORM rotates geometry.

***LOAD LS-DYNA version 971 R6.0.0.**

Keyword: *CONTROL_ADAPTIVE

Fixed problem when *CONTROL_ADAPTIVE and *LOAD_SEGMENT/*LOAD_SEGMENT_SET are used together for 2D analysis; problem was the effect of *LOAD_SEGMENT i disappeared after adaptive step.

Keyword: *LOAD_BLAST_ENHANCED

When BLAST=4 in *LOAD_BLAST_ENHANCED, eliminate ground encounter when determining which entity is first hit by a shock wave. Use correct time parameters and scaled distance so velocity decay is correctly computed for encounter with the ground reflected wave.

Keyword: *LOAD_BLAST_ENHANCED

Fixed blast wind velocity and wave index for BLAST=4.

Keyword: *LOAD_BLAST_ENHANCED

Reported the minimum computed arrival time.

Keyword: *LOAD_BLAST_ENHANCED

Fixed an index problem for the blast origin when multiple charges are defined. This problem elicited false warning messages during initialization and had no ill effect on the actual blast load.

Keyword: *LOAD_RIGID_BODY

Added warning message if *LOAD_RIGID_BODY part is a slave part in *CONSTRAINED_RIGID_BODIES.

Keyword: *LOAD_SSA

Fixed problem of incorrectly reading in explosive charge definitions.

Keyword: *LOAD_THERMAL_VARIABLE_BEAM

Fixed problem of *LOAD_THERMAL_VARIABLE_BEAM giving wrong temperatures for tubular sections.

Keyword: *DEFINE_CONNECTION_PROPERTIES

Fixed case of AREA EQ.ne.0:
The true area was not correctly used in the failure function,
if the exponents EXSN, EXSB, EXSS were not 1.0.

Keyword: *EOS_...

Added input check for duplication of EOS ID.

Keyword: *MAT_...

Fixed incorrect experimental curve data output to curveplot file for
materials 76, 77, 134, 175, 176, 178 and 276.

Keyword: *MAT_CRUSHABLE_FOAM

Fixed instability problem of *MAT_CRUSHABLE_FOAM for plain strain analysis.

Keyword: *MAT_NONLOCAL

Modified nonlocal failure for thick shells so that if elements are stacked,
averaging will not occur with elements on the top and bottom, only those
on the side.

Keyword: *MAT_USER_DEFINED_MATERIAL_MODELS

Fixed plane strain and axisymmetric elements when used with orthotropic
user-defined materials. This fix affects shell forms 13, 14, 15, 43,
44, 52, 53. The wrong strain and stress transformation was being done.

Keyword: *MAT_019

Made the strain rate the first history variable after the
plastic strain for all versions of *MAT_STRAIN_RATE_DEPENDENT_PLASTICITY.

Keyword: *MAT_021

Modified *MAT_ORTHOTROPIC_THERMAL so that it works with angles on the
*SECTION_SHELL or *SECTION_TSHELL card to define material directions
for layers.

***MAT LS-DYNA version 971 R6.0.0.**

Keyword: *MAT_024

Made beam *MAT_PIECEWISE_LINEAR_PLASTICITY plasticity iteration consistent i with *MAT_PLASTIC_KINEMATIC (*MAT_003).

Keyword: *MAT_024 and others

Improved user-defined failure subroutine template matusr_24 including passing of updated strain.

Keyword: *MAT_034

Made fabric material forms 12, 13, and 14 output global stress to the d3plot file like the other fabric forms and other materials.

Keyword: *MAT_036

Corrected bad output of strains and thickness reduction to d3plot for *MAT_3-PARAMETER_BARLAT.

Keyword: *MAT_036, *MAT_190

A bug fixed for these materials in the case of equi-biaxial stretching.

Keyword: *MAT_058, *MAT_158

Enabled the negative AOPT (*DEFINE_COORDINATE_NODES) option for *MAT_LAMINATED_COMPOSITE_FABRIC and *MAT_RATE_SENSITIVE_COMPOSITE_FABRIC.

Keyword: *MAT_072R3

Made updates to *MAT_CONCRETE_DAMAGE_REL3 per KCSE.

Keyword: *MAT_072R3

Implemented updates from KCSE for *MAT_CONCRETE_DAMAGE_REL3.

Keyword: *MAT_082

Fixed bug in *MAT_PLASTICITY_WITH_DAMAGE_ORTHO for brick elements and 2D solids which caused elements to spuriously vanish.

Keyword: *MAT_098

Fixed bug in *MAT_SIMPLIFIED_JOHNSON_COOK for implicit.

Keyword: *MAT_100

Made *MAT_SPOTWELD/SIGY<0 consistent with *MAT_SPOTWELD/SIGY>0.

Keyword: *MAT_100

Fixed for damage calculation in *MAT_SPOTWELD_DAMAGE-FAILURE when SIGY<0.

Keyword: *MAT_100

Fixed the BETA>0 option for brick or brick assembly spot welds that use DMGOPT=2, 10, 11, and 12. Weld failure was not occurring after damage initialization.

Keyword: *MAT_107

Fixed in Zerilli-Armstrong law in *MAT_MODIFIED_JOHNSON_COOK

Keyword: *MAT_120, *MAT_120_JC

Added extra history variable 16 to *MAT_GURSON and *MAT_GURSON_JC for convenience in checking against GISSMO damage model.

Keyword: *MAT_123

Fixed RTCL damage of *MAT_MODIFIED_PIECEWISE_LINEAR_PLASTICITY_RTCL such the input parameter EPS0 is now used correctly.

Added parameter TRIAX which is a limit on the triaxiality, beyond which damage will not grow.

Keyword: *MAT_124

Implemented an optional Young's modulus for compression in *MAT_PLASTICITY_COMPRESSION_TENSION.

Keyword: *MAT_125

Fixed energy calculation in *MAT_KINEMATIC_TRANSVERSELY_ANISOTROPIC.

***MAT LS-DYNA version 971 R6.0.0.**

Keyword: *MAT_156, 221, 226, 232, 233, 244, 267

Fixed various material model bugs in
*MAT_MUSCLE (for truss elements),
*MAT_ORTHOTROPIC_SIMPLIFIED_DAMAGE,
*MAT_KINEMATIC_HARDENING_BARLAT89,
*MAT_BIOT_HYSTERETIC,
*MAT_CAZACU_BARLAT,
*MAT_UHS_STEEL,
*MAT_EIGHT_CHAIN_RUBBER

Keyword: *MAT_169

Added new option to *MAT_ARUP_ADHESIVE: If parameter BTHK<0, then do not modify time step. This helps to avoid very small time steps, but it can affect stability.

Keyword: *MAT_172

Modified *MAT_CONCRETE_EC2 so that when *INTEGRATION_SHELL or *PART_COMPOSITE is used, the AOPT-related angle is recalculated for each integration point.
The standard LS-DYNA treatment is to get the AOPT-related angle from the first IP made of an orthotropic material, then use the same angle for subsequent points.

Keyword: *MAT_174

Fixed output of curvature to "plastic strain" position in output of *MAT_RC_BEAM.

Keyword: *MAT_181

Fixed instability of *MAT_SIMPLIFIED_RUBBER/FOAM in full deck restart.

Keyword: *MAT_187

Fixed for large curve IDs in *MAT_SAMP-1.

Keyword: *MAT_224

Added *MAT_TABULATED_JOHNSON_COOK for type 13 tetrahedon.

Keyword: *MAT_233

Fixed NUMINT option of *MAT_CAZACU_BARLAT.

Added new options related to rate effects and damage.

Keyword: *MAT_234

Fixed calculation of sound speed for *MAT_VISCOELASTIC_LOOSE_FABRIC.

Include element number when writing out failure message.

Keyword: *MAT_244

Implemented *MAT_UHS_STEEL for 2D solid elements.

Keyword: *MAT_244

Added option to *MAT_UHS_STEEL for automatic switching between cooling and heating algorithm based on the temperature slope.

Fixed scaling of heat flow due to phase transitions in *MAT_UHS_STEEL.

Added thermal scale factor to *MAT_UHS_STEEL.

Support heating and/or reheating of *MAT_UHS_STEEL. The heat equation is taken from Oddy et al (1996) Microstructural Predictions Including Arbitrary Thermal Historic ReAustinitization And Carbon Segregation Effects.

Keyword: *MAT_272

Improved *MAT_RHT, including automatic parameter generation.

Keyword: *MAT_ADD_EROSION

Fixed GISSMO damage history output to d3hsp.

Keyword: *MAT_ADD_EROSION

Modified GISSMO parameters SHRF and BIAXF.

***MAT LS-DYNA version 971 R6.0.0.**

Keyword: *MAT_..._THERMAL

Corrected calculation of heat flux vector for orthotropic materials.

Keyword: *MAT_THERMAL_USER_DEFINED

Corrected temperature in user materials in combination with 2D solids.

Corrected history variable handling in thermal user materials.

Keyword: *PART_COMPOSITE

Enabled *PART_COMPOSITE to work with material types 104, 108, 122, 133, 135, 137, 157, 223, 226, 229, 233, 234, 235, and 242. Previous, a keyword error was reported.

Keyword: *SECTION_SOLID, *MAT_...

Improved accuracy of type 13 (pressure-averaged) tetrahedron.

Modified several existing material models for type 13 tetrahedron, including *mat_015, *mat_098, *mat_106, *mat_224.

Keyword: Various *MAT_... including *MAT_ADD_EROSION

Fixed for NUMINT<0 in materials 120, 123, 187, 224, and GISSMO: solid elements are now deleted directly after 1st IP fails, i.e., input value of NUMINT is ignored.

Keyword: *ALE_FAIL_SWITCH_MMG

Supported ALE Multimaterial Group switching for failed material in MPP.

Keyword: *ALE_FSI_PROJECTION

Fixed bug affecting this command in MPP.

Keyword: *ALE_AMBIENT_HYDROSTATIC, *INITIAL_HYDROSTATIC_ALE

For these commands, add in support for *EOS_GRUNEISON but at significant cost owing to an iterative algorithm.

Keyword: *CONTROL_ALE

Invoked preferred multi-material ALE advection method for explosive simulations by setting DCT = -1.

Keyword: *CONTROL_ALE, *EOS_JWL

Initialized the *EOS_JWL pressure with PREF and the relative volume (ALE formulation).

Keyword: *CONTROL_EXPLOSIVE_SHADOW_SET

Implemented this feature for MPP.

Keyword: *CONSTRAINED_LAGRANGE_IN_SOLID

Fixed PFACMM=3 option.

Keyword: *DATABASE_GLSTAT, *DATABASE_MATSUM, *DATABASE_ALE_MAT

Improved writing of internal energy for ALE parts.

Keyword: *DATABASE_FSI

Corrected the computation of the mass flux.

Keyword: *INITIAL_STRESS_DEPTH

Initialized the stress for each ALE group.

SPH LS-DYNA version 971 R6.0.0.

Keyword: *CONTROL_SPH

Updated strain calculation (due to circumferential velocity) for SPH axisymmetry option.

Keyword: *CONTROL_SPH, *DEFINE_SPH_TO_SPH_COUPLING

Implemented SPH CONT=1 and SPH-to-SPH coupling for MPP.

Keyword: *DEFINE_SPH_TO_SPH_COUPLING

Fixed read error for multiple *DEFINE_SPH_TO_SPH_COUPLING.

Keyword: *MAT_072, _173, _241

Added *MAT_072 for SPH.

Added *MAT_MOHR_COULOMB for SPH but no support for material's LOCAL=1 option.

Added *MAT_JOHNSON_HOLMQUIST_JH1 for SPH.

Keyword: *SECTION_SPH

Output bulk viscosity energy of SPH as hourglass energy.

Keyword: *SECTION_SPH

Updated bulk viscosity of SPH for MPP to conserve the total energy.

Keyword: *..._SPH

Fixed bugs related to SPH with thermal solver.

Keyword: *MAT_267

Added EFG compatibility to the *MAT_EIGHT_CHAIN rubber model.

*IMPLICIT LS-DYNA version 971 R6.0.0.

Keyword: *BOUNDARY_CYCLIC

Fixed MPP implicit implementation of cyclic symmetry boundary conditions.

Keyword: *CONTROL_IMPLICIT_AUTO

Fixed bug in implicit auto time stepping combined with keypoints.

Keyword: *CONTROL_IMPLICIT_AUTO

Fixed bug when using thermal dependent materials and auto time stepping in implicit.

Keyword: *CONSTRAINED_JOINT, *CONTROL_RIGID

Fixed issues with the SMP and MPP implementations of the implicit (LM) joints.

Keyword: *CONTROL_IMPLICIT_CONSISTENT_MASS

Fixed bug in *CONTROL_IMPLICIT_CONSISTENT_MASS (MPP only).

Keyword: *CONTROL_IMPLICIT_GENERAL

Properly handled the switching between explicit to implicit in the case of large rotations of rigid bodies.

Keyword: *CONTROL_IMPLICIT_CONSISTENT_MASS

Added consistent mass matrices for solid types 1, 2, 10, 15; beam type 1, 2, 3, 4, 5.

Keyword: *CONTROL_IMPLICIT_EIGENVALUE

Fixed stress output for implicit mode shapes.

Fixed improper handling of *CASE for implicit eigenvalue analysis.

Keyword: *CONTROL_IMPLICIT_...

Fixed the output to implicit databases (d3eigv, d3mode, d3iter) for 10-noded tetrahedra.

Fixed MPP writing of d3eigv for large problems.

Keyword: *CONTROL_IMPLICIT_SOLUTION

Bug fixed in implicit nonlinear solver 12.

Keyword: *CONTROL_IMPLICIT_STATIC_CONDENSATION

Fixed bug of incorrectly sorted nodes for
*CONTROL_IMPLICIT_STATIC_CONDENSATION.

Keyword: *CONSTRAINED_JOINT_...

Fixed handling of joints in the presence of curve-based implicit switching.

Keyword: *DATABASE_SPCFORC

Fixed output of spc forces in implicit.

Keyword: *DATABASE_option

Fixed incorrect output to spcforc for implicit.

Fixed MPP Implicit error in collecting and reporting forces due to certain constraints.

Keyword: *ELEMENT_DISCRETE

Disabled velocity dependent dampers for implicit static solution.

Keyword: *INTERFACE_LINKING_...

Fixed MPP Implicit's treatment of *INTERFACE_LINKING_... to match the year old changes to this feature for MPP Explicit.

Keyword: *MAT_054, *MAT_055

Enabled implicit solutions with solids comprised of
*MAT_ENHANCED_COMPOSITE_DAMAGE.

Keyword: n/a

Tuned up implicit memory requirements output.

Keyword: *SECTION_BEAM, *CONTROL_IMPLICIT_GENERAL

Stiffness matrix of type 2 beam was broken when IGS=1 (geometric stiffness).

Thermal LS-DYNA version 971 R6.0.0.

Keyword: *CONSTRAINED_SPOTWELD

The 2 nodes identified by this keyword will be constrained to the same temperature in a thermal only problem or in a coupled thermal mechanical problem.

Keyword: *CONTROL_THERMAL_SOLVER, *MAT_244

The parameter TSF (thermal speedup factor) on the *CONTROL_THERMAL_SOLVER keyword will automatically scale the kinetic rate equations used in *MAT_UHS_STEEL. TSF is used for time scaling, such as when the punch speed is artificially increased when modeling metal stamping operations.

Keyword: *MAT_172, *MAT_ADD_PERMEABILITY

Fixed bug whereby *MAT_CONCRETE_EC2 beams and shells did not respond to temperature change in a coupled thermal/structural analysis.
Pore pressure analysis thermal expansion was also failing to respond to temperature change in a coupled analysis.

Keyword: *BOUNDARY_PRESCRIBED_MOTION_RIGID

Fixed MPP problem related to *BOUNDARY_PRESCRIBED_MOTION_RIGID when used with relative motion.

Fixed for MPP d3plot output, which was not honoring the IEVERP flag on *DATABASE_EXTENT_BINARY.

Keyword: *CONTROL_MPP_DECOMPOSITION

Enhanced decomposition option to allow isolate and distribute for multiple parts or part set.

Keyword: *CONTROL_MPP_DECOMPOSITION_SHOW, *AIRBAG_PARTICLE

Fixed problem of viewing MPP decomposition when particle method is invoked.

Keyword: *ELEMENT_DIRECT_STIFFNESS_MATRIX

Enhanced MPP performance of explicit with superelements for large number of processes and small number of superelements.

Keyword: *ELEMENT_SEATBELT_SLIPRING

Fixed problem in MPP with sliprings having "optional orientation node".

Keyword: *LOAD_SURFACE_STRESS

Added MPP support of *LOAD_SURFACE_STRESS.

Keyword: *MAT_NONLOCAL

Added support for *MAT_NONLOCAL in MPP.

Keyword: n/a

Improved commonality between SMP and MPP in rigid body routines.

Forming LS-DYNA version 971 R6.0.0.

Keyword: *CONTROL_FORMING_SCRAP_FALL

Allowed displacement control of trim steel kinematics.

Fixed bug in scrap constraints release when trim steel is moving in local coordinate system

Keyword: *DEFINE_CURVE_TRIM_3D

Improved flanging simulation by allowing the user to control how far the elements from a defined curve can be selected for mesh refinement.

Keyword: *DEFINE_CURVE_TRIM_NEW

Improved 2D trimming: allow trimming curves to cross the part boundary many times.

Fixed a bug in trimming where SPC constraints could be lost.

Keyword *INTERFACE_COMPENSATION_NEW

Fixed bugs in springback compensation:

- 1)rigid tooling now can be the exact same size as the deformed blank;
- 2)improvement in springback compensation with undercut;
- 3)blank can now be bigger than the rigid tool.

*INTERFACE_COMPENSATION_NEW now allows multiple regions to be compensated at the same time, with keyword

*DEFINE_CURVE_COMPENSATION_CONSTRAINT_BEGIN
and *DEFINE_CURVE_COMPENSATION_CONSTRAINT_END.

Discrete Element Method LS-DYNA version 971 R6.0.0.

Keyword:

Fixed DEM to DEM contact in MPP.

Keyword: *CONTACT_NODES_TO_SURFACE

Supported part/part set input in N2S contact with discrete element sphere.

Keyword: *DEFINE_DE_TO_SURFACE_COUPLING

Included rotational DOF for discrete element to surface coupling.

Keyword: *ELEMENT_DISCRETE_SPHERE

Added capillary force to simulate wet particles for Discrete Sphere Element. The particle-particle and particle-segment capillary force is calculated based on Langmuir 2005, 12, 10992-10997

Added rolling friction for discrete sphere element.

Isogeometric Elements LS-DYNA version 971 R6.0.0.

Keyword: *ELEMENT_SHELL_NURBS_PATCH

Allowed degenerated nurbs-patches (multiple control-points at the same physical location) for isogeometric elements.

Keyword: *ELEMENT_SHELL_NURBS_PATCH

Made the transformation of parametric coordinates to physical coordinates of interpolation nodes compatible with MPP.

Fixed post-processing of stresses, ... via interpolation elements in case of multiple nurbs patches that share common edges.

Keyword:

Fixed interactive "cross" command in Material Model Driver.

Keyword: *BOUNDARY_USA_SURFACE

Added USA support for implicit.

Keyword: *CASE

Allowed *KEYWORD_JOBID and *CASE together.

Keyword: *CONTROL_ADAPTIVE

Fixed error in adaptivity restart if any elements have failed.

Keyword: *DAMPING_FREQUENCY_RANGE

Fixed bug whereby damping applied was much greater than the input value if $FHIGH/FLOW < 3.16$

Keyword: *DAMPING_PART_STIFFNESS

Fixed bug when damping is enabled in *DAMPING_PART_STIFFNESS and rayleigh damping energy is computed per RYLEN=2 in *CONTROL_ENERGY; shells may have had spurious stresses.

Keyword: *DEFINE_FUNCTION

Accommodated triangular segments in pressure loading using *DEFINE_FUNCTION.

Keyword: *DEFINE_BOX_LOCAL

Fixed bug affecting LOCAL option of *DEFINE_BOX.

Keyword: *DEFINE_CURVE_FUNCTION

Fixed a bug which gave null results for the translational velocity and acceleration functions (VX,VY,VZ,AX,AY,AZ) when the optional local coordinate system N3 was specified.

Miscellaneous LS-DYNA version 971 R6.0.0.

Keyword: *DEFORMABLE_TO_RIGID_AUTOMATIC

Fixed problem of *DEFORMABLE_TO_RIGID_AUTOMATIC not switching correctly for MPP.

Keyword: *DEFORMABLE_TO_RIGID_AUTOMATIC

Fixed bug affecting D2R automatic switching in MPP wherein small variations of contact forces between tire and road in a tire rolling example were observed.

Keyword: *INCLUDE_TRANSFORM

Fixed *INCLUDE_TRANSFORM with *PART_CONTACT or *PART_COMPOSITE_CONTACT:
Decay constant DC was not transformed correctly.

Fixed *AIRBAG_HYBRID with *INCLUDE_TRANSFORM.

Fixed *MAT_034 (negative LCUA, LCUB, LCUAB) with *INCLUDE_TRANSFORM:
Scaling with FCTMAS, FCTTIM, and FCTLEN was not done correctly in this case.

Fixed *MAT_183 with *INCLUDE_TRANSFORM.

Fixed *CONTACT_... parameter CID_RCF (Optional Card C):
Offset IDDOFF from *INCLUDE_TRANSFORM was not accounted for.

Fixed *MAT_100 with SIGY<0: Account for offset from *INCLUDE_TRANSFORM.

Fixed *CONSTRAINED_JOINT_STIFFNESS and offsets from INCLUDE_TRANSFORM.

Fixed temperature conversion in *INCLUDE_TRANSFORM including
h conversion in *BOUNDARY_CONVECTION and adding FtoR and RtoF.

Keyword: *INITIAL_FOAM_REFERENCE_GEOMETRY

Calculated nodal mass and d3hsp mass properties of parts based on initial foam reference geometry instead of deformed geometry at initial state.

Miscellaneous LS-DYNA version 971 R6.0.0.

Keyword: *PART_ANNEAL

Added *PART_ANNEAL for MPP. Zeroes stress in part at specified time.

Keyword: *..._PORE_AIR

Corrected a bug for the restart of pore air simulation

Keyword: *SENSOR_DEFINE_FORCE

Corrected bug for MPP version of sensor_define_force.

Keyword: *SENSOR_DEFINE_NODE

Cleaned up direction specification syntax for sensor.

Keyword: *SENSOR_DEFINE_NODE

Fixed incorrect behaviour when VID=Y/Z in *SENSOR_DEFINE_NODE and DIR=Y/Z in *DEFINE_COORDINATE_NODES.

Keyword: *SET_PART_LIST_GENERATE

Fixed bug of *SET_PART_LIST_GENERATE not recognizing *PART_COMPOSITE.

Keyword: *SET_SEGMENT_GENERAL

Allowed *SET_SEGMENT_GENERAL for element formulations that have midside nodes.

Keyword: *SET_PART_LIST_GENERATE

Fixed bug affecting *SET_PART_LIST_GENERATE when *PART_MOVE is present (null set was created).

Keyword: *SET_..._COLLECT

Fixed bug for *SET_SEGMENT_COLLECT and attributes of *SET_*_COLLECT. All attributes of *SET_PART_COLLECT, *SET_NODE_COLLECT and *SET_SHELL_COLLECT were not copied to the new set.

Keyword: *TERMINATION_SENSOR

Terminate right after sensor-switch status is changed.

Keyword: *TERMINATION_SENSOR, *INTERFACE_SPRINGBACK_LSDYNA

Write dynain file when termination is due to *TERMINATION_SENSOR.

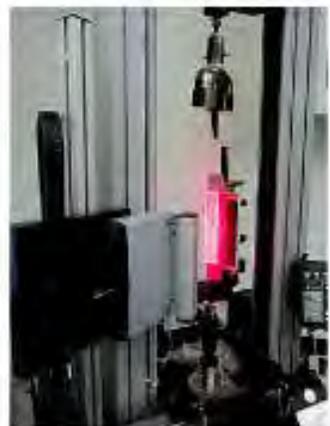
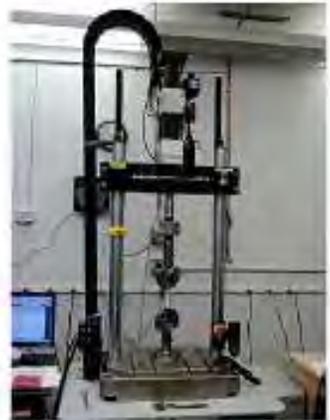
DatapointLabs Mechanical Test Capabilities



DatapointLabs has greatly expanded its mechanical test capabilities:

- **New Bidirectional Video Extensometer:** We have installed a new advanced video extensometer (AVE) with the capability to simultaneously measure linear and transverse strains during a stress-strain measurement. The extensometer greatly enhances our non-contact capability, making high quality measurements to large strains needed for hyperelastic rubber testing and film properties. Strains can be captured during cyclic experiments, rendering it possible to capture Mullins effects in rubber materials. The transverse strain measurement capability allows us to measure Poisson's ratio of soft materials such as rubber, foam and films. Transverse strains can also be measured in the plasticity region providing data for high end material models such as LS-DYNA's [SAMP-1](#).
- **New Test Frames for Fatigue:** We have added two servo-hydraulic test frames to double our fatigue testing capability. At this time, we can perform fatigue measurements on a wide range of materials, from metals and plastics to weak materials such as rubber and foam. These new additions will increase our ability to provide fatigue data more efficiently.
- **New Test Frame for Rubber, Films and Fiber:** We have added an electro-mechanical test frame which allows for high extension testing suitable for rubber, films, and fibers. The test frame is coupled with a large extension environmental test chamber which permits us to greatly increase the range of measurement strains when stress-strain data are needed at elevated and low temperatures.

Keep an eye on our [catalog](#) for new tests.





BETA CAE Systems S.A.– ANSA

Is an advanced multidisciplinary CAE pre-processing tool that provides all the necessary functionality for full-model build up, from CAD data to ready-to-run solver input file, in a single integrated environment. ANSA is a full product modeler for LS-DYNA, with integrated Data Management and Process Automation. ANSA can also be directly coupled with LS-OPT or LSTC to provide an integrated solution in the field of optimization.

BETA CAE Systems S.A.– μETA

Is a multi-purpose post-processor meeting diverging needs from various CAE disciplines. It owes its success to its impressive performance, innovative features and capabilities of interaction between animations, plots, videos, reports and other objects. It offers extensive support and handling of LS-DYNA 2D and 3D results, including those compressed with SCAI's FEMZIP software



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The Cray XMT supercomputing system is a scalable massively multithreaded platform with a shared memory architecture for large-scale data analysis and data mining. The system is purpose-built for parallel applications that are dynamically changing, require random

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The Cray CX1000 series is a dense, power efficient and supremely powerful rack-mounted supercomputer featuring best-of-class technologies that can be mixed-and-matched in a single rack – creating a customized hybrid computing platform to meet a variety of scientific workloads.

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Testing over 1000 materials per year for a wide range of physical properties, DatapointLabs is a center of excellence providing global support to industries engaged in new product development and R&D.

The company meets the material property needs of CAE/FEA analysts, with a specialized product line, TestPaks®, which allow CAE analysts to easily order material testing for the calibration of over 100 different material models.

DatapointLabs maintains a world-class testing facility with expertise in physical properties of plastics, rubber, food, ceramics, and metals.

Core competencies include mechanical, thermal and flow properties of materials with a focus on precision properties for use in product development and R&D.

Engineering Design Data including material model calibrations for CAE Research Support Services, your personal expert testing laboratory Lab Facilities gives you a glimpse of our extensive test facilities Test Catalog gets you instant quotes for over 200 physical properties.



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Invention Suite™

Invention Suite™ is an enterprise-level CAE software solution, enabling concept to product. Invention's first set of tools will be released soon, in the form of an advanced Pre & Post processor, called PreSys.

Invention's unified and streamlined product architecture will provide users access to all of the suite's software tools. By design, its products will offer a high performance modeling and post-processing system, while providing a robust path for the integration of new tools and third party applications.

PreSys

Invention's core FE modeling toolset. It is the successor to ETA's VPG/PrePost and FEMB products. PreSys offers an easy to use interface, with drop-down menus and toolbars,

increased graphics speed and detailed graphics capabilities. These types of capabilities are combined with powerful, robust and accurate modeling functions.

VPG

Advanced systems analysis package. VPG delivers a unique set of tools which allow engineers to create and visualize, through its modules--structure, safety, drop test, and blast analyses.

DYNAFORM

Complete Die System Simulation Solution. The most accurate die analysis solution available today. Its formability simulation creates a "virtual tryout", predicting forming problems such as cracking, wrinkling, thinning and spring-back before any physical tooling is produced



Visual-Crash

Visual Crash for LS-DYNA helps engineers perform crash and safety simulations in the smoothest and fastest possible way by offering an intuitive windows-based graphical interface with customizable toolbars and complete session support. Being integrated in ESI Group's Open VTOS, an open collaborative multi-disciplinary engineering framework, Visual-Crash for DYNA allows users to focus and rely on high quality digital models from start to finish. Leveraging this state of the art environment, Visual Viewer, visualization and plotting solution, helps analyze LS-DYNA results within a single user interface.

vibro-acoustic software

With ESI's vibro-acoustic software you no longer have to account for noise and vibration right at the design stage - no more costly delays or panic driven test-

based solutions. Our vibro-acoustic software has everything you need to diagnose potential noise and vibration problems up front in your development process. Manage risk by identifying possible problem areas that may need more detailed modeling or test based development, while you still have time to make an impact on the product!

VA One

VA One is a complete solution for simulating the response of vibro-acoustic systems across the full frequency range. VA One seamlessly combines Finite Elements (FE), Boundary Elements (BEM) and Statistical Energy Analysis (SEA) in ONE model. It is the only simulation code on the market today that contains the complete spectrum of vibro-acoustic analysis methods within ONE common environment.



Participant Solutions
GNS - Gesellschaft für Numerische Simulation mbH

www.gns-mbh.com

Animator4

A general finite element post-processor and holds a leading position in its field. Animator4 is used worldwide by almost all automotive companies, a great number of aerospace companies, and within the chemical industry.

Generator2.

A specialized pre-processor for crashworthiness applications and has become very successful in the field of passenger safety and pedestrian protection. It is mainly used as a positioning tool for finite element component models by a great number of automobile companies throughout the world.

Indeed

An easy-to-use, highly accurate virtual manufacturing software that specializes in the simulation of sheet metal forming processes. Indeed is part of the GNS software suite and works concurrently with all other GNS software products.

OpenForm

A pre- and post-processor independently of a particular finite element forming simulation package. The software is extremely easy to handle and can be used as was designed to enable those who are not finite element experts to carry out multi-stage forming simulations with even complex multi purpose finite element codes.



Gompute is owned, developed and operated by Gridcore AB in Sweden. Founded in 2002, Gridcore is active in three areas: Systems Integration, Research & Development and HPC as a service.

Gridcore has wide experience of different industries and applications, developed a stable product portfolio to simplify an engineer/scientist's use of computers, and has established a large network of partners and collaborations, where we together solve the most demanding computing tasks for our customers. Gridcore has offices in Gothenburg

(Sweden), Stuttgart (Germany), Durham NC (USA) and sales operations in The Netherlands and Norway.

The Gridcore developed E-Gompute software for internal HPC resources gives end users (the engineers) an easy-to-use and complete environment when using HPC resources in their daily work, and enables collaboration, advanced application integrations, remote pre/post, accounting/billing of multiple teams, license tracking, and more, accelerating our customers usage of virtual prototyping.



Participant Solutions
JSOL Corporation

www.jsol.co.jp/english/cae/

HYCRASH

Easy-to-use one step solver, for Stamping-Crash Coupled Analysis. HYCRASH only requires the panels' geometry to calculate manufacturing process effect, geometry of die are not necessary. Additionally, as this is target to usage of crash/strength analysis, even forming analysis data is not needed. If only crash/strength analysis data exists and panel ids is defined. HYCRASH extract panels to calculate it's strain, thickness, and map them to the original data.

JSTAMP/NV

As an integrated press forming simulation system for virtual tool shop the JSTAMP/NV meets the various industrial needs from the areas of automobile, electronics, iron and steel,

etc. The JSTAMP/NV gives satisfaction to engineers, reliability to products, and robustness to tool shop via the advanced technology of the JSOL Corporation.

JMAG

JMAG uses the latest techniques to accurately model complex geometries, material properties, and thermal and structural phenomena associated with electromagnetic fields. With its excellent analysis capabilities, JMAG assists your manufacturing process



LS-DYNA

A general-purpose finite element program capable of simulating complex real world problems. It is used by the automobile, aerospace, construction, military, manufacturing, and bioengineering industries. LS-DYNA is optimized for shared and distributed memory Unix, Linux, and Windows based, platforms, and it is fully QA'd by LSTC. The code's origins lie in highly nonlinear, transient dynamic finite element analysis using explicit time integration.

LS-PrePost

An advanced pre and post-processor that is delivered free with LS-DYNA. The user interface is designed to be both efficient and intuitive. LS-PrePost runs on Windows, Linux, and Macs utilizing OpenGL graphics to achieve fast rendering and XY plotting.

LS-TaSC™

A Topology and Shape Computation tool. Developed for engineering analysts who need to optimize structures, LS-TaSC works with both the implicit and explicit solvers of LS-DYNA. LS-TaSC handles topology optimization of large non-linear problems, involving dynamic loads and contact conditions.

LSTC Dummy Models

Anthropomorphic Test Devices (ATDs), as known as "crash test dummies", are life-size mannequins equipped with sensors that measure forces, moments, displacements, and accelerations.

LSTC Barrier Models

LSTC offers several Offset Deformable Barrier (ODB) and Movable Deformable Barrier (MDB) model



Oasys LS-DYNA® Environment

The Oasys Suite of software, exclusively written for LS-DYNA®, is at the leading edge of the market and is used worldwide by many of the largest LS-DYNA® customers.

Oasys PRIMER

Oasys PRIMER is a model preparation tool that is fully compatible with the latest version of LS-DYNA®, eliminating the risk of data loss or corruption when a file is manipulated, no matter what operations are performed on it:

Key benefits:

- Maintains data integrity
- Finds and fixes model errors (currently over 5000 checks)
- Specialist tools for dummy positioning, seatbelt fitting, mechanisms, interior head impact etc.
- Connection manager for spotwelds, bolts, adhesive etc.
- Intelligent editing, deletion and merging of data
- Customisable with macros and JavaScript.

Oasys D3PLOT

Oasys D3PLOT is a powerful 3D visualization package for post-processing LS-DYNA® analyses

Key benefits:

- Fast, high quality graphics
- Easy, in-depth access to all LS-DYNA® results.
- User defined data components
- Customisable with JavaScript.

Oasys T/HIS

Oasys T/HIS is an X-Y graph plotting package for LS-DYNA®

Key benefits:

1. Automatically reads all LS-DYNA® results.
2. Wide range of functions and injury criteria.
3. Easy handling of data from multiple models
4. Scriptable for automatic post-processing

Oasys REPORTER

Oasys REPORTER is an automatic report generation tool, for use with LS-DYNA®, which allows fast automatic report creation for analyses.



Center of Excellence

Hengstar Technology is the first LS-DYNA training center of excellence in China. As part of its expanding commitment to helping CAE Engineers, Hengstar Technology will continue to organize high level training courses and seminars in 2012.

The lectures/training are taught by senior engineers and experts mainly from LSTC, Carhs, OEMs, and other consulting groups.

On Site Training

Hengstar also provides customer customized training programs on-site at the company facility. Training is

tailored for company needs using LS-DYNA or the additional software products by LSTC.

Distribution & Support

Hengstar Distributes and supports LS-DYNA, LS-OPT, LS-PrePost, LS-TaSC. Hongsheng Lu, previously was directly employed by LSTC before opening his distributorship in China for LSTC software. He travels to LSTC often to keep current on the latest software features and support to continue to grow Hengstar as a CAE consulting group.



Participant Solutions

Products

ANSA	TestPaks®	LS-PrePost	CRAY XE6m™
Inventium Suite™	CRAY XK6	HYCRASH	LS-TaSC™
Animator 4	TOYOTA THUMS	CRAY XE6™	PreSys
CRAY CX1000™	Visual Crash	Generator 2	VPG
JMAG	VA One	DYNAFORM	LSTC Dummy Models
LS-DYNA	CRAY Sonexion 1300™	Indeed	Vibro-Acoustic Software
OpenForm		Oasys Primer	
JSTAMP/NV	GOMPUTE Cloud		LSTC Barrier Models
Oasys D3Plot	μETA		Oasys T/HIS



North America
Distribution – Consulting

United States

DYNAMAX
www.dynamax-inc.com

sales@dynamax-inc.com

LS-DYNA
 LSTC Dummy Models

LS-OPT

LS-PrePost
 LSTC Barrier Models

LS-TaSC

United States

CAE Associates Inc.
www.caeai.com

info@caeai.com

ANSYS Products

CivilFem

Consulting ANSYS
 Consulting LS-DYNA

United States

Predictive Engineering
www.predictiveengineering.com

george.laird@predictiveengineering.com

FEMAP
 LS-PrePost

NX Nastran
 LS-TaSC

LS-DYNA
 LSTC Dummy Models
 LSTC Barrier Models

LS-OPT

Europe
Distribution – Consulting



France	Alliance Svce. Plus - AS+ www.asplus.fr/ls-dyna	v.lapoujade@asplus.fr		
	LS-DYNA	LS-OPT	LS-PrePost	LS-TaSC
	DYNAFORM	VPG	MEDINA	
	LSTC Dummy Models		LSTC Barrier Models	
France	ALYOTECH www.alyotech.fr	nima.edjtemai@alyotech.fr		
	ANSYS	LS-DYNA	MOLDEX3D	FEMZIP
	Primer	PreSys	DYNAFORM	SKYGEN
	MERCUDA	MOCEM		
Germany	CADFEM GmbH www.cadfem.de	lsdyna@cadfem.de		
	ANSYS	LS-DYNA	optiSLang	DIGIMAT
	ESAComp	AnyBody	VPS	
	FTI FormingSuite			
Germany	DYNAMore GmbH www.dynamore.de	uli.franz@dynamore.de		
	ANSYS	LS-DYNA	optiSLang	DIGIMAT
	LS-OPT	LS-PrePost	LS-TaSC	DYNAFORM
	Primer	D-Spex	GENESIS	FEMZIP
	VisualDoc		LSTC Dummy & Barrier Models	
			TOYOTA THUMS	
Germany	GNS www.gns-mbh.com	mbox@gns-mbh.com		
	Animator	Generator	Indeed	OpenForm
Netherland	Infinte www.infinite.nl	j.mathijssen@infinite.nl		
	ANSYS Products	CivilFem	CFX	Fluent
	LS-DYNA	LS-PrePost	LS-OPT	LS-TaSC



Europe Distribution – Consulting

Italy	EnginSoft SpA www.enginsoft.it		info@enginsoft.it	
	ANSYS CADfix ESAComp AdvantEdge	MAGMA LS-DYNA AnyBody Straus7	Flowmaster Dynaform FTI Software LMS Virtual.Lab	FORGE Sculptor ModeFRONTIER
Russia	STRELA		info@dynarusia.com	
	LS-DYNA LSTC Dummy Models	LS-TaSC	LS-OPT LSTC Barrier Models	LS-PrePost
Sweden	DYNAmore Nordic www.dynamore.se		marcus.redhe@dynamore.se	
	ANSA LS-PrePost FormingSuite	μETA LS-TaSC	LS-DYNA FastFORM LSTC Dummy Models LSTC Barrier Models	LS-OPT DYNAform
Sweden	GRIDCORE www.gridcore.se		info@gridcore.com	
	LS-DYNA Cloud Service		Additional software Additional Services	
Switzerland	DYNAmoreSwiss GmbH www.dynamore.ch		info@dynamore.ch	
	LS-DYNA LS-TaSC		LS-OPT LSTC Dummy Models LSTC Barrier Models	LS-PrePost
UK	Ove Arup & Partners www.oasys-software.com/dyna		dyna.sales@arup.com	
	LS-DYNA LS-TaSC REPORTER DIGIMAT	PRIMER SHELL Simpleware	LS-OPT D3PLOT FEMZIP LSTC Dummy Models LSTC Barrier Models	LS-PrePost T/HIS HYCRASH



China **ETA – China** lma@eta.com.cn
www.eta.com/cn

Inventium	VPG	DYNAFORM	NISA
LS-DYNA	LS-OPT	LSTC Dummy Models	LS-PrePost
		LSTC Barrier Models	LS-TaSC

China **Oasys Ltd. China** Stephen.zhao@arup.com
www.oasys-software.com/dyna

PRIMER	D3PLOT	HYCRASH	T/HIS	REPORTER	SHELL
LS-DYNA		LS-OPT	LSTC Dummy Models		LS-PrePost
DIGIMAT		FEMZIP	LSTC Barrier Models		LS-TaSC

China **Shanghai Hengstar Technology** info@hengstar.com
www.hengstar.com

LS-DYNA	LS-TaSC	LSTC Barrier Models	
LS-DYNA Courses	LS-OPT	LSTC Dummy Models	LS-PrePost

**Asia Pacific
Distribution – Consulting**



Japan	ITOCHU www.engineering-eye.com	Ls-dyna@ctc-g.co.jp		
	LS-DYNA LSTC Dummy Models	LS-OPT LSTC Barrier Models	LS-PrePost CmWAVE	LS-TaSC

Japan	JSOL www.jsol.co.jp/english/cae			
	JSTAMP LS-DYNA LSTC Dummy Models	HYCRASH LS-OPT LSTC Barrier Models	JMAG LS-PrePost	LS-TaSC

Japan	FUJITSU http://jp.fujitsu.com/solutions/hpc/app/lodyna			
	LS-DYNA LSTC Dummy Models	LS-OPT LSTC Barrier Models	LS-PrePost CLOUD Services	LS-TaSC



Asia Pacific Distribution – Consulting

Korea

THEME

wschung@kornet.com

www.lsdyna.co.kr

LS-DYNA
LSTC Dummy Models
eta/DYNAFORM
JSTAMP/NV
FEMZIP

LS-OPT
LSTC Barrier Models
FormingSuite
Scan IP

LS-PrePost
eta/VPG
Simblow
Scan FE

LS-TaSC
Planets
TrueGRID
Scan CAD

Korea

KOSTECH

young@kostech.co.kr

www.kostech.co.kr

LS-DYNA
LSTC Dummy Models
eta/DYNAFORM
AxStream

LS-OPT
LSTC Barrier Models
DIGIMAT
TrueGrid

LS-PrePost
eta/VPG
Simuform
FEMZIP

LS-TaSC
FCM
Simpack

Taiwan

Flotrend

gary@flotrend.tw

www.flotrend.com.tw

LS-DYNA
LSTC Dummy Models

LS-OPT
LSTC Barrier Models

LS-PrePost
eta/VPG

LS-TaSC
FCM

Cloud Services including LS-DYNA



Japan Fujitsu www.fujitsu.com

Germany Gridcore www.gridcore.se

Sweden Gridcore www.gridcore.se

United States Gompute www.gompute.com



To Join FEA Distribution/Consultants

PARTICIPATION

Participation is available in this section, for only this section or for full participation.

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Contact Anthony agiac99@aol.com for further information.



The Complete Courses Offered Can Be Found At: www.cadfem.de

Please check the site for accuracy and changes. Among the many course offered:

Introduction to simulation with ANSYS

Workbench

03/13/12

Introduction to simulation with Diffpack

03/22/12 11/06/12

Introduction to explicit structural mechanics
with ANSYS-LS-DYNA and LSTC's LS-
DYNA

02/08/12 05/09/12
08/29/12 09/05/12
11/06/12 12/19/12

Working efficiently with Diffpack in ANSYS
Workbench

03/23/12 11/07/12

Introduction to simulation of joint- and muscle-
forces with AnyBody

04/25/12 09/19/12

Material Modeling with LS-DYNA

03/06/12 10/16/12

Efficient coupling of AnyBody with ANSYS
Workbench

04/27/12 09/21/12

Simulation of composites with ANSYS

Composites PrepPost and LS-DYNA

05/08/12 08/21/12

Additional Courses are offered – please check
the website for upcoming dates for: FTI

Forming Suite - DIGIMAT

DIFFPACK and others.

Contact modeling with LS-DYNA

05/22/12 11/06/12

Modeling joints with LS-DYNA

03/02/12 10/12/12

Individual Training: Take advantage of the
expertise of our specialists and get to know
how simulation processes in your company can
be arranged in an optimal way.

Crash simulation with LS-DYNA

09/25/12



Germany

DYNAmore

The Complete Courses Offered Can Be Found At: www.dynamore.de/en

Intro LS-DYNA	03/19/12 09/27/12
03/12/12 04/19/12 04/25/12 06/18/12	
09/20/12 10/15/12 10/30/12 12/10/12	Dummy Modeling
	06/14/12
Contact Definitions	
03/16/12 10/18/12	Airbag Modeling
	06/14/12
Element types	
07/04/12	eta/DYNAFORM
	03/17/12 09/17/12
Plasticity	
10/24/12	Metal Forming
	03/29/12
Users Interfaces	
11/19/12	ALE
	10/11/12
Crash Analysis	
04/17/12 12/04/12	Meshless Methods
	10/11/12
Spot Welds	



The Complete Courses Offered Can Be Found At: www.lstc.com

Please check the site for accuracy and changes.

Among the many course offerings are the following:

Smoothed Particle Hydrodynamics (SPH) in
LS-DYNA and Element-Free Galerkin (EFG)
CA

February 23-24, 2012

March 20-21, 2012

Implicit Analysis with LS-DYNA CA

March 22-23, 2012

Contact in LS-DYNA CA

March 15-16, 2012

Advanced Impact Using LS-DYNA MI

April 24-26, 2012

Introduction to LS-PrePost (no charge) MI

March 19, 2012

Introduction to LS-PrePost (no charge) CA

April 30, 2012

Introduction to LS-DYNA MI

March 20-23, 2012

Introduction to LS-DYNA CA

May 1-4, 2012

Advanced Options in LS-DYNA CA



Sweden

DYNAmore Nordic

The Complete Courses Offered Can Be Found At: www.dynamore.se

Please check the site for accuracy and changes.

Among the many course offerings are the following:

LS-PrePost 3, introduction

March 12, 2012

Anders Jernberg Fars Hatt,

Kungälv

LS-DYNA, implicit analysis

March 27, 2012

Dr. Thomas Borrvall

Linköping

LS-DYNA, introductory course

March 13, 2012

Dr. Jimmy Forsberg Fars Hatt,

Kungälv

LS-DYNA, Simulation of sheet metal forming processes

April 17, 2012

Dr. Mikael Schill

Linköping

ANSA & Metapost, Introductory course

March 20, 2012

David Karlsson

Linköping

LS-DYNA, Material modelling

April 24, 2012

Dr. Thomas Borrvall

Linköping

ANSA CFD Meshing

March 22, 2012

David Karlsson

Linköping

France

Alliance Plus (AS+)



The complete Training Courses offered can be found at www.asplus.fr/ls-dyna
Please check the site for accuracy and changes.

LS-DYNA Explicit/Implicit solver – Special University Training session (to be held in Toulouse) 15-18/02 – Special University Price (date to be confirmed)	LS-DYNA Advanced Implicit Solver 25/09
Other regular courses (in Paris) ...	LS-DYNA ALE / FSI 19-20/03 & 22-23/10
LS-DYNA Introduction Explicit Solver 10-12/09	LS-DYNA SPH 21-22/05 & 8-9/10
LS-DYNA Introduction Implicit Solver 24/09	LS-PrePost 3.0 – Advanced meshing capabilities 5/04 & 27/09 & 29/11
LS-DYNA Unified Introduction Implicit & Explicit Solver 16-19/01, 18-21/06 & 12-15/11	LS-DYNA User Options 23-24/05
LS-OPT & LS-TaSC Introduction 21-22/03 & 24-25/10	LS-DYNA – Plasticity, Damage & Failure – By Paul DU BOIS 26-27/11 (date may be changed in Q1)
Switch to LS-DYNA 2-3/04 & 10-11/10	LS-DYNA – Polymeric materials – By Paul DU BOIS 12-13/12
Switch from Ls-PrePost 2.X to 3.X 4/04 & 26/09 & 28/11	LS-DYNA – Geo-material modeling 14-15/12



United States

Engineering Technology Associates

The Complete Courses Offered Can Be Found At: www.eta.com

Please check the site for accuracy and changes.

Among the many course offering are the following:

Introduction to DYNAFORM

03/06-07/2012

04/03-04/2012

05/01-02/2012

Introduction to PreSys

03/13/2012

04/10/2012

05/08/2012

Introduction to LS-DYNA

03/20-21/2012

04/17-18/2012

05/15-16/2012



The Complete Courses Offered Can Be Found At: www.caeai.com

Please check the site for accuracy and changes. Among the many course offering are the following:

ANSYS Training, CFD and FEA Consultants Serving CT, NJ, NY, MA, NH , VT

Apr 12, 2012 2 days

Introduction to CivilFEM
Middlebury, CT

Jun 11, 2012 1 day

ANSYS DesignModeler
Middlebury, CT

Apr 16, 2012 3 days

Introduction to ANSYS Mechanical APDL Part
I (Traditional GUI
Middlebury, CT

Jun 16, 2012 2 days

Introduction to ANSYS Mechanical
(Workbench)
Middlebury, CT

Apr 19, 2012 2 days

Introduction to ANSYS Mechanical APDL Part
II (Traditional GUI)
Middlebury, CT

May 14, 2012 1 day

ANSYS Workbench Meshing for CFD
Middlebury, CT

May 15, 2012 2 days

Introduction to CFX
Middlebury, CT



United States

Paul Du Bois & Len Schwer

PAUL DU BOIS & LEN SCHWER

Announce their annual LS-DYNA® training class schedule

May 2012 - Somerset Inn - Troy Michigan

These popular LS-DYNA training classes have been offered since 2006, in North America and Europe. The classes continuously evolve, reflecting the ongoing additions and improvements in LS-DYNA's simulation capabilities.

Paul du Bois and Len Schwer, Co-Instructors:

<i>Penetration Modeling with LS-DYNA</i>	May 1 - 2 (Tuesday – Wednesday)
<i>Blast Modeling with LS-DYNA</i>	May 3 - 4 (Thursday – Friday)
<i>Modeling and Simulation with LS-DYNA</i>	May 7 - 8 (Monday - Tuesday)

Len Schwer, Instructor:

<i>Concrete & Geomaterial Modeling</i>	May 9 - 10 (Wednesday - Thursday)
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Class descriptions available on the LSTC web site: www.lstc.com/training

To request Registration Form, please send email to: schwerdubois@yahoo.com



The Complete Courses Offered Can Be Found at www.hengstar.com

2012	2	3	4	5	6	7	8	9	10	11	12
An Introduction to LS-DYNA(High Level)											
Concrete & Geomaterial Modeling with LS-DYNA											
Pedestrian Safety and Bonnet Design with LS-DYNA											
Crashworthiness Theory and Technology											
LS-DYNA MPP, Airbag Simulation with LS-DYNA											
Introduction of LS-OPT which is Based on LS-DYNA											
Passive Safety and Restraint Systems Design											
Crashworthiness Simulation with LS-DYNA											
Passive Safety Simulation with LS-DYNA											
Crashworthy Car Body Development - Design, Simulation and Optimization											



France

Alyotech Technologies

For course location visit www.alyotech.fr

LS-DYNA Introduction

April 03-05
June 04-06
Sept 10-12
Oct 01-03
Nov 12-14
Dec 03-05

LS-DYNA Thermal

Sept 13-14

LS-DYNA Implicit

May 21-23
Sept 17-19
Nov 19-21

LS-PrePost – Meshing

May 24
Sept 27
Nov 26

LS-PrePost – New Interface

May 25
Sept 28
Nov 27

LS-OPT Introduction

June 18-19
Dec 10-11

LS-TaSC – Topology Optimization

June 20
Dec 12

**Material Modeling & User Defined
Material in LS-DYNA**

July 10-11

Crash & Impact Modeling

April 02-05

FSI & ALE in LS-DYNA

March 15-16

LS-DYNA Composite

July 12-13

Oasys LS-DYNA 5th Annual Update Meetings India

April 17th & 19th 2012

Pune – Tuesday, 17th April 2012

The Ista Hotel, 88 Nagar Road, Adjacent to Aga Khan Palace Pune.

Bangalore – Thursday, 19th April 2012 – The Taj Vivanta, Whitefield, Bangalore.

Oasys Ltd and nHance Engineering Solutions Pvt Ltd are pleased to announce the 5th Oasys LS-DYNA Update meetings in India for the year 2012. First meeting shall be held at Pune on Tuesday 17th April 2012 at The Ista Hotel and second meeting shall be held at Bangalore on Thursday 19th April 2012 at The Taj Vivanta, Whitefield.

Each of these is a full day free of charge event covering both LS-DYNA and Oasys software and is a perfect opportunity to find out about current and future developments and how the software is being used in the engineering community.

The presentations will mainly cover latest features of LS-DYNA software, Oasys suite and presentations from industry members specifically from OEMs. This year's presentations also include presentation from Mr. Yun Huang, LSTC on the implicit capabilities of LS-DYNA for NVH and Durability. Detailed agenda shall be published next month.

Presentations of the last year Update Meeting can be seen at http://www.oasys-software.com/dyna/en/events/users_india_apr-11/users_india_apr-11.shtml.

Registration: Please send your registration to this event by email to india.support@arup.com with your name, company/affiliation, telephone number and your choice for event.

Venue: If you plan to stay over before or after the event, we are pleased to confirm that we have negotiated a special rate for attendees of the Oasys LS-DYNA Update meeting. Please contact us for assistance.

Contact Details: If you have any queries regarding this event you can contact:

Mr. Asif Ali:
nhance Engineering Solutions(P)Ltd (Part of the ARUP Group)
Plot No. 39, Ananth Info Park, HiTec City-Phase 2
Madhapur, Hyderabad-500081,India
Tel: +91 (0) 40 44369797/8 Email:
india.support@arup.com

Compute User Group Meeting (7th Edition)

May 08 & 09, 2012

<http://www.simdi.se/>

Location:

Scandic Crown Hotel
Gothenburg (Sweden)

About the Compute User Meeting

The Compute User Meeting, formerly called SIMDI (Simulation and Data intensive Fair), is an event that gathers different actors of the Simulation Industry

Primarily GUM11 gathers users of Gompute® software suite and the Gompute on Demand™ service but it is open to any other person interested in the application of numerical simulation on their daily work.

This year meeting is the sixth one all of them has been celebrated in Gothenburg Sweden.

Gompute on Demand delivers HPC on demand for technical and scientific applications, it is owned and

operated by Gridcore AB, a Swedish System integrator specialized in technical and scientific computing.

You may get more information about gompute and Gridcore at www.gompute.com and www.gridcore.se .

GUM11's Agenda Manager

Iago Fernandez
Phone: +46 704 19 39 76
Mail: iago.fernandez@se.gompute.com

GUM11's Event Manager

Anne-Marie Ohlsson
Phone: +46 31 18 21 60
Mail: amo@gridcore.se

12th International LS-DYNA Users Conference

June 03-05, 2012

Conference website: www.ls-dynaconferences.com

12th Int'l LS-DYNA Users Conference
June 3rd, 4th & 5th

Training 6th & 7th

Conference Plenary/Keynote Addresses

June 4th

Professor Thomas J.R. Hughes

The University of Texas

Professor David J. Benson

University of California

Mr. Kenji Takada

Honda Japan

Mr. Paul A. Du Bois

Consulting

FEA Information Participants

Sponsoring and/or exhibiting:

- ARUP
- CRAY
- BETA CAE Systems, S.A.
- DatapointLabs
- ESI North America
- ETA
- Gompute Inc.
- GNS mbH
- D3View
- FEA Information
- JSOL

Hotel - Venue - Reservations

Hyatt Regency Dearborn

Fairlane Town Center, Dearborn, MI 48126

Please inform reservations that you're attending the LS-DYNA Conference

For booth, sponsorships or any conference questions contact: info@lst.com

TRAINING OFFERED:

- Pre- Conference LS-PrePost
- Pre- Conference User Material Dev. In LS-DYNA
- Advanced ALE Applications
- ALE/Eulerian & FSI
- Blast & Penetration Using LS-DYNA
- Heat Transfer with Warm Forming and Hot Stamping Applications
- Introduction to LS-OPT
- NVH & Frequency Domain Analysis w/ LS-DYNA
- Occupant Restraint: Dummies/Barriers
- Polymeric Material With LS-DYNA
- Probabilistic Design Using LS-OPT & LS-DYNA
- SPH & Element-Free Galerkin

GNS – 7th OpenFOAM® Workshop

June 25th 2012

<http://www.openfoamworkshop.org/2012/OFW7.html>

7th OpenFOAM® Workshop

The 7th OpenFOAM® Workshop will be held in Darmstadt (next to Frankfurt, Germany) from June 25-28, 2012 - hosted by the Center of Smart Interfaces (CSI) and the Graduate School of Computational Engineering (GSCE) of the Technische Universität Darmstadt.

The OpenFOAM® Workshop intends to bring together OpenFOAM®'s developers and users, to promote collaborative activities, exchange information and share experiences in similar areas of interest. The 7th OpenFOAM® Workshop is

- a community forum and open discussion platform for OpenFOAM® users and developers,

- the largest OpenFOAM® community event of the world (expected 400 participants),
- since 2006: sustainable, community-driven and non-profit.

The 7th OpenFOAM® Workshop is organized using the Community Portal of the Extend Project.

Please visit for abstract submission, registration and program schedule.

Your OpenFOAM®-Workshop Organizing Committee

committee@openfoamworkshop.org

October 09, 2012

<http://www.dynamore.de/en/training/conferences/upcoming/ls-dyna-forum-2012/ls-dyna-update-forum-2011>

German LS-DYNA Forum 2012

LS-DYNA Forum, 9 - 10 October 2012, Ulm, Germany

On the 9th and 10th October 2012, our 11th LS-DYNA Forum will be taking place at the Maritim Hotel in Ulm, Germany. We cordially invite you not only to attend the event but submit a paper. In your presentation, you can talk about your experiences with LS-DYNA or LS-OPT and you can discuss and exchange these experiences with other users.

User presentations will form the core of the event. General lectures given by renowned speakers are also planned as well as talks on the latest LS-DYNA und LS-OPT .

Comprehensive information all about LS-DYNA software can be obtained from the accompanying exhibition.

The Forum will be accompanied by seminars which will be held during the week of the conference on the subjects of CPM Airbag OoP, ALE and fluid-

structure inter-action, meshless methods and on concrete and geomaterial modeling.

Your presentation: You are cordially invited to contribute towards the program plan by submitting a paper. Contributions from the various areas of application of LS-DYNA/LS-OPT are planned

To Submit your papers: Please send us the title, authors and a short summary (approx. 300 words).

Dates: Submission of proposed paper:
25th May 2012

Author notification: 11th June 2012

Submission of two-page summary for proceedings:
7th Sept. 2012

Location: Maritim Hotel Ulm
Basteistraße 40, 89073 Ulm

Registration and contact

DYNAmore GmbH

Tel. +49 (0) 7 11 - 45 96 00 - 0

Fax +49 (0) 7 11 - 45 96 00 - 29

E-Mail: forum@dynamore.de

www.dynamore.de/forum12

**ANSYS Conference
& 30. CADFEM Users' Meeting
October 24-26, 2012**

Location: Kassel Germany

Environmental protection and economic aspects make electric mobility one of the great challenges of the coming years. Step-by-step it will replace traditional forms of mobility in everyday life. Therefore, a number of projects have been defined in so-called 'model regions' in order to better understand and optimize this process.

For a better understanding of electric mobility and its optimization, simulation specialist ANSYS has extended its portfolio with a set of simulation applications that can serve as models in the development and implementation of innovative drive concepts. Structural and fluid mechanics and electromagnetic simulation models of the individual components are modeled in a consistent environment both individually and interacting,

considering the drive as a complete multi-physical system – Engineering the System!

The ANSYS Conference & the 30th CADFEM Users' Meeting focus on the many simulation options in electric mobility and several other current application fields where structural mechanics, fluid mechanics and electro magnetics issues are important.

CADFEM GmbH and ANSYS Germany GmbH cordially invite you to join the conference

We look forward to your participation

The CADFEM & ANSYS Germany Team

Events - Conferences

Conference - Event

start date

04/03 Germany	Automotive CAE Grand Challenge 2012 www.carhs.de/grand-challenge
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04/16 Belgium	11th Int'l Conf. - Computer Applications/Information Tech. -Maritime Ind. www.compit.info/
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05/15 US	2012 SIMULIA Customer Conference www.3ds.com/company/events/scc-2012/overview/
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05/21 Germany	Nastran Users Meeting http://pages.mscsoftware.com/NastranUserMeeting2012-Home.html
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06/11 USA	AMD Fusion12 Developer Summit http://www.amd.com
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06/12 US	Seventh M.I.T. Conference www.seventhmitconference.org/
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ESI-group

<http://www.esi-group.com/corporate/news-media/press-releases/2012-english-pr/esi-releases-the-latest-version-of-ace-plus-suite-multiphysics-and-cfd-software>

ESI releases the latest version of ACE+ Suite, the Multiphysics and Advanced CFD software improves product development processes for Automotive to Semiconductor industries

CRAY

<http://investors.cray.com/phoenix.zhtml?c=98390&p=irol-newsArticle&ID=1667153&highlight=>

Cray's YarcData Division Launches New Big Data Graph Appliance

The uRiKA graph appliance fills an unmet need in the rapidly-growing Big Data market.

BETA CAE Systems S.A.

announces the release of ANSA v13.2.2 with new features and known problems resolved

http://www.beta-cae.gr/news/20120222_announcement_ansa_v13.2.2.htm

The official software release is comprised by the latest ansa_v13.2.2 files that reside in the server at the time of this announcement. These replace any pre-releases and files downloaded prior to March 22nd, 2012.

BETA CAE Systems S.A.

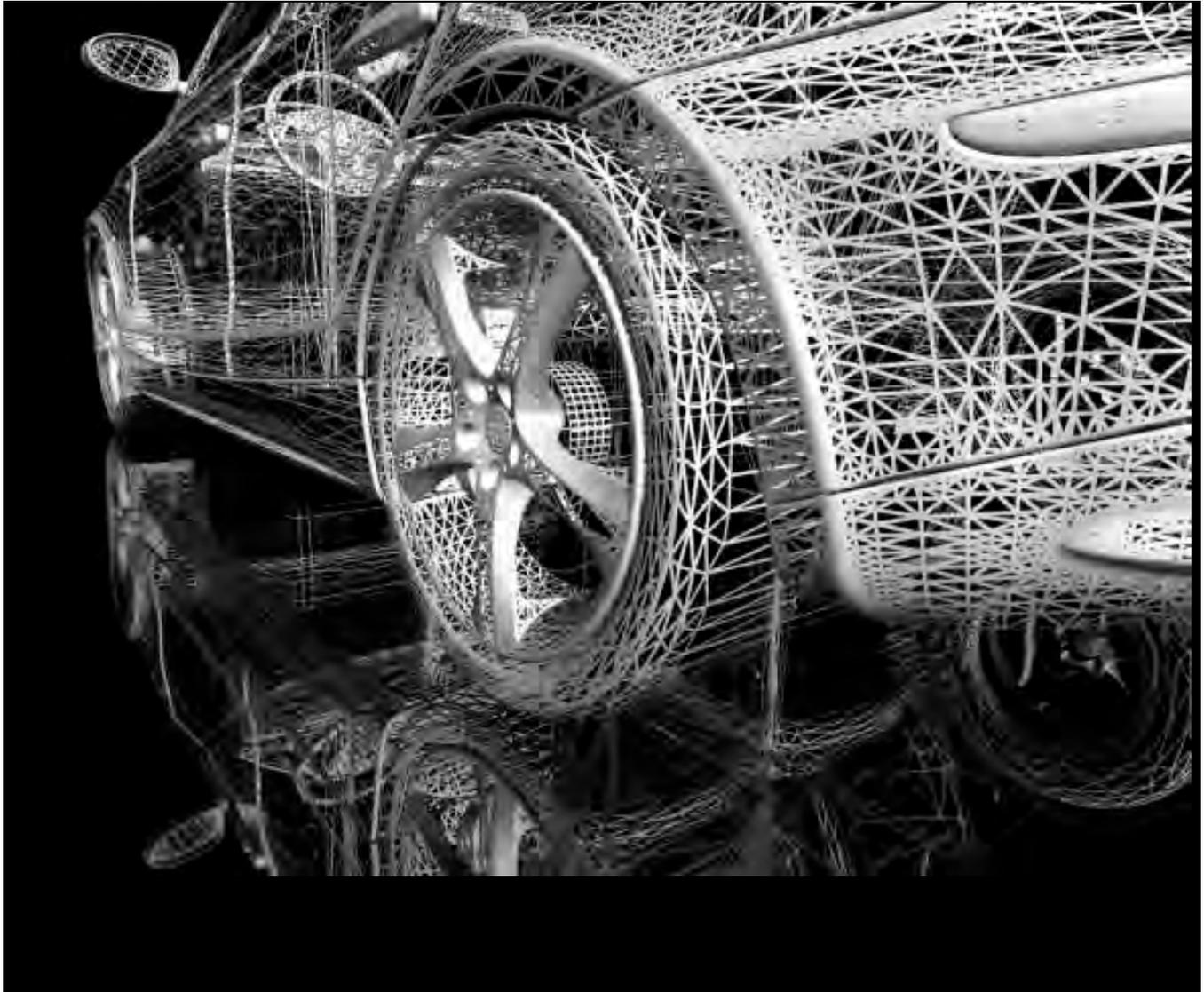
announces the release of μ ETA v6.8.0 with new important features and code corrections

http://www.beta-cae.gr/news/20120222_announcement_meta_v6.8.0.htm

The official software release is comprised by the latest meta_post_v6.8.0 files dated March 20th, 2012. These replace any pre-releases and files downloaded prior to this date.

FEA Information Engineering Journal

Volume 1, Issue 2, March 2012





FEA Information Engineering Journal

Contents – About The Author

FEA Information Engineering Journal Publications

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Prediction of Springback in CNC Tube Bending Process Based on Forming Parameters

Levent Sözen, Mehmet A. Guler, Recep M. Görgülüarslan, Engin M. Kaplan
- University of Economics and Technology

Process Modeling of Freeform Incremental Forming Using LS-DYNA®

Feng Ren, Zhen Cui, and Z. Cedric Zia Ford Motor Company

Numerical Simulation and Experimental Study of Electromagnetic Forming

Kianhui Shang, Larry Wilkerson, Steve Hatkevich; American Trim LLC
Pierre L'Eplattenier,, LCTC

Published in the 11th International LS-DYNA® Users Conference 2010 Proceeding.

Publications at this time are internet available.

www.feapublications.com

Publications focus on a set of criteria, among them being:

- FEA Analysis focusing on LS-DYNA® .
 - (LS-DYNA is a registered trademark of Livermore Software Technology Corp.)
- Information, or papers not previously published, that are of technical interest.
- Published papers from alternative publications, that we have authorization to showcase.

For Information on publishing a paper contact mv@feainformation.com

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